## OPTIMAL MULTIPLE DISTRIBUTION GENERATION PLACEMENT IN MICROGRID SYSTEM



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1

# **1. Introduction**

Microgrid (MG), a system of multiple distributed generations (DG) to serve loads, can reduce the system loss and improve system reliability.



**Figure 1.1 Microgrids** 

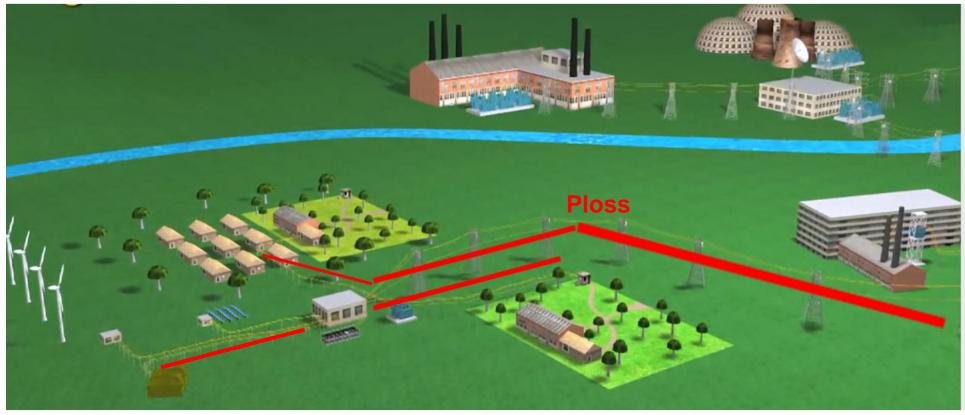
# **1. Introduction**

## In this thesis, there are 2 contributions as:

- For optimal multiple DG placement by improved reinitialized social structures PSO (IRS-PSO) to minimize the total real power loss, MG with four different types of DG is introduced.
- The IRS-PSO is developed to solve optimal multiple DG placement by adding reinitialized particles to escape from local optimum in the process of velocity updating when particle velocity is not within limit.

# 2. Research objective

To determine optimal location and size of multiple distributed generations by IRS-PSO for minimizing the total real power loss in a MG system.



# **3. Optimal multiple DG placement in MG**

## **3.1 Literature reviews**

Optimal distributed generation (DG) placement, a mixed integer nonlinear programming problem, has been solved by various methods including repetitive load flow, genetic algorithm (GA), and traditional basic particle swarm (BPSO) in refs. (Mahat P., 2006), (Mithulanthan N., 2004), and (Kuersuk W., 2006) to minimize the total real power loss in a MG system. However, the problem of all methods is premature convergence because of local traps.

## **3.1 Literature reviews (continuous)**

In this chapter, The total real power loss calculated by Backward-Forward sweep method, is minimized by Improved reinitialized social structures PSO (IRS-PSO) determining the optimal multiple DGs placement in the MG system. Its solutions are compared to BPSO, Adaptive weight PSO (APSO), and Global best, local, Neighbor - PSO (GLN-PSO).

## **3.2 Objective function**

Minimize P<sub>loss</sub>

P. Location

$$P_{loss} = \sum_{i=1}^{n} \sum_{j=1}^{n} A_{ij} (P_i P_j + Q_i Q_j) + B_{ij} (Q_i P_j - P_i Q_j)$$
(3.2)

where,  $P_i$  and  $P_j$  are the real power injection at bus i and j.  $Q_i$  and  $Q_j$  are the reactive power injection at bus i and j.  $A_{ij}$  and  $B_{ij}$  are distribution coefficients which are discussed as following

$$A_{ij} = \frac{R_{ij}\cos(\delta_i - \delta_j)}{V_i V_j}$$
(3.3)

$$B_{ij} = \frac{R_{ij}\sin(\delta_i - \delta_j)}{V_i V_j}$$
(3.4)

where,  $R_{ij}$  is the distribution resistance between bus i and j.  $V_i$  and  $V_j$  are the voltage at — bus i and j.  $\delta_i$  and  $\delta_j$  are the voltage angle at bus i and j.

7

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(3.1)

## **3.2 Objective function (continue)**

Subject to:

(a) Power balance constraint

$$\sum_{i} P_{DG,i} = \sum_{i} P_{D,i} + P_{loss}$$
(3.5)  
where,  $P_{DG,i}$  and  $P_{D,i}$  are the DG and demand power at bus  $i$ .

#### (b) Voltage limits

$$\left| \mathcal{V}_{i} \right|^{\min} \leq \left| \mathcal{V}_{i} \right| \leq \left| \mathcal{V}_{i} \right|^{\max} \tag{3.6}$$

where,  $|V_i|^{\min}$  and  $|V_i|^{\max}$  are the minimum and maximum voltage at bus i.

#### (c) Real power generation limits

$$P_{DG,i}^{\min} \le P_{DG,i} \le P_{DG,i}^{\max} \tag{3.7}$$

<u>where</u>,  $P_{DG,i}^{\min}$  and  $P_{DG,i}^{\max}$  is the minimum and maximum DG real power at bus i.

(d) Reactive power generation limits

$$Q_{DG,i}^{\min} \le Q_{DG,i} \le Q_{DG,i}^{\max}$$
(3.8)

where,  $Q_{DG,i}^{\min}$  and  $Q_{DG,i}^{\max}$  is the minimum and maximum DG reactive power at bus i.

#### Microgrid models

Type 1 - MG with DG supplying real power only

 $P_i = P_{DGj} - P_{Dj}$ 

Type 2 - MG with DG supplying reactive power only

$$Q_i = Q_{DGj} - Q_{D,i}$$

DG like synchronous condenser will provide reactive power to improve the voltage profile.



(3.9)



(3.10)

Type3 - MG with DG supplying real and consuming reactive power

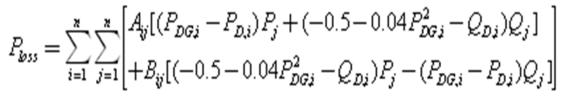
 $Q_{DG,i} = -(0.5 + 0.04 P_{DG,i}^2)$ 

The real power loss can be given as follows;



(3.11)

(3.12)



#### Type 4 - MG with DG regulating the bus voltage

In this type, DG supplying real power injection by the DG will require reactive power to support the bus voltage.

#### Type 5 - MG with four different types of DGs

Photovoltaic, synchronous condenser, wind generation, and biomass generator representing each type of DG are considered.



## Practical swarm optimization (PSO)

- PSO is a population based search method with position of particle is representing solution and swarm of particles as searching agent. This idea is similar to bird flocks searching for food.
- Bird = a particle
- Food = a solution



# **3.3 Optimal multiple DG placement by Improved reinitialized social structures PSO (IRS-PSO)**

- The IRS-PSO is used for optimal DG placement. Initially, the particles represent DG sizes and locations which will be randomly initialized at the first iteration and reinitialize at every certain number of iterations. Reinitializing is used to escape from local optimum by totally randoming particles except *gbest*.
- The velocity and particle position equations of IRS-PSO are (3.18) and (3.19). The IRS-PSO velocity includes an inertia term, a cognitive term *pbest*, and three social terms including *gbest*, *lbest*, and *nbest*.

$$v_{i,d}^{k+1} = w^{k} v_{i,d}^{k} + C_{p} R_{i} (pbest_{i,d}^{k} - x_{i,d}^{k}) + C_{g} R_{2} (gbest_{d}^{k} - x_{i,d}^{k}) + C_{i} R_{3} (lbest_{i,d}^{k} - x_{i,d}^{k}) + C_{n} R_{4} (nbest_{i,d}^{k} - x_{i,d}^{k})$$
(3.18)

where,  $C_p$ ,  $C_g$ ,  $C_l$ , and  $C_n$  are the personal, global best, local, and near neighbor acceleration.  $R_1$ ,  $R_2$ ,  $R_3$ , and  $R_4$  are random numbers in the range [0,1].  $pbest_{i,d}^k$ ,  $gbest_d^k$ ,  $lbest_{i,d}^k$ , and  $nbest_d^k$  are the personal, global best, local, and near neighbor of dimension dat iteration k.

Particle positions are updated by

$$x_{i,d}^{k+1} = x_{i,d}^k + v_{i,d}^{k+1}$$
(3.19)

• For optimal multiple DGs placement by IRS-PSO, the procedure can be described in 10 steps as follows.

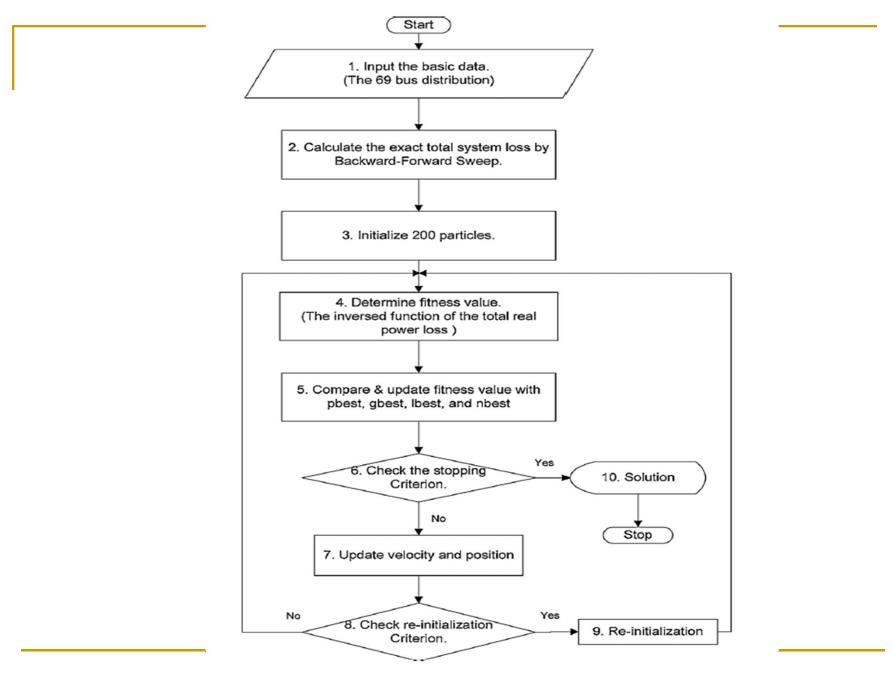


Figure 3.1 The flowchart of IRS-PSO for optimal multiple DGs placement 14

## **3.4 The test system**

A MG distribution system (22 kV) is used as a test system. The 69 radial bus distribution MG system has a total load of 3.80 MW and 2.69 MVAR (Baran ME, 1989). The single line diagram of the test system is shown in Figure 3.2. When multiple small DGs are optimally placed, the bus voltage limits are set to 0.90 and 0.98 per unit. For the minimum and maximum sizes of DG, real power generation limits are set to 0.05 and 5 MW, and reactive power generation limits are set to 0.05 and 5 MVAR.

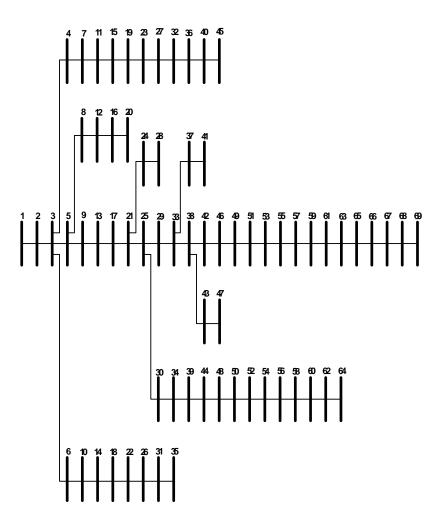


Figure 3.2 The single line of the test system

# 4. Numerical results

- Tables 1 4 show optimal DG locations and sizes minimizing real power loss in 69 bus distribution system. The maximum number of DG is set to 3. The decrease in total real power loss will depend on the location and size of DG. As shown in Tables 1 4, IRS-PSO total real power losses are less than repetitive load flow for each type of one DG. In Table 3.4, IRS-PSO total losses are less than BPSO, APSO, and GLN-PSO of three DGs. Moreover, MG type 4 gives the minimum loss since it can supply real and reactive power. IRS-PSO in MG type 4 can reduce loss by 97.25%.
- In Table 5 (MG type 5), different DG types are considered in MG. There are three combinations of DG types 1 and 2, types 1 3, and types 1 4. Apparently, the IRS-PSO is the best method for optimal placement because of minimum real power loss. Moreover, IRS-PSO total losses are less than BPSO, APSO, and GLN-PSO of three and four DGs.

Method		Bus no.	DG size	Bus no.	DG size	Bus no.	DG size	Ploss	Qloss	Loss re	duction %
			(MW)		(MW)		(MW)	(kW)	(kVAR)	Real	Reactive
		The ori	ginal power lo	ss in the 69 bu	s system			230.1962	104.4490		
IRS-PSO		56 56 56	1.8739 1.7799 1.7147	55 55	0.5342 0.3761	33	0.5304	84.7804 73.0659 70.7626	41.2841 36.6217 35.6308	63.17 68.26 69.26	60.47 64.94 65.90
	4 7	11 15	19 23	27 32 36	40 45						
	8	12 16		28 37	41						PO
1 2 	3 5 9	13 17	21 25	29 33 3	3 42 46	49 51 5	3 55 57	59 61 63	65 66	67 68	<b>69</b>
		1 1		' <b>O</b> '	43 47				1 1	1 1	
		1 1		30 34 39		50 52 5	4 56 58	60 62 64	1 1	1 1	

Method	В	us no.	s no. DG size (MVAR)		no.	DG size	Bus n	0.	DG size		Plos		Qlo		Loss	reduction %
			(MVAR)			(MVAR)			(MVAR)		(kW)	)	(kV/	AR)	Real	Reactiv
		The orig	zinal power l	oss in th	e 69 bu	s system				1	230.19	62	104.4	490		
RS-PSO		56 56 56	1.3306 1.2683 1.2025		8 51	0.5464 0.2332	33		0.3707		155.33 149.85 148.38	74	71.9 64.6 69.1	481	32.52 34.90 35.54	33.32
ſ	4 7	11 15	19 23	27 3	2 36	40 45										5-4)
	8	12 16	20 24	28	37	41							1-1		2 1.1	
	5 9	13 17	21 25	29 3	3 38	42 46 43 47	49 51	53	55 57	59   	61	63	65 e	6 67	68	69 
				30 3	4 39	44 48	50 52	54	56 58	60	62	64				
	6 10	14 18	22 26	31 3	5											

				Table	e III.	Optim	al DG	place	ement	in N	1G wit	th DG	suppl	ying r	eal po	ower a	ind co	nsumi	ng rea	ctive	power					
Method				Bus no.		DG		I	Bus no	0.		size	I	Bus no	).	DG			Ploss			loss		Loss	redu	ction %
						(M)	VA)				(1)	(VA)				(M	VA)		( <b>kW</b> )		(K	VAR)		Real		Reactive
IRS-PSO				Th 56 56 56	e origi	nal po 1.69 1.58 1.51	28 98	oss in	the 6 51 49	9 bu		em 800 647		25		0.71	130	1	30.19 03.061 92.220 91.500	16 )3	49 45	.4490 .3193 .4009 .5127		55.23 59.94 60.25		52.78 56.53 57.38
		4	7	11	15	19	23	27	32	36	40	45										1				1
			8	12	16	20	24	28	[	37	41															
	3	5	9	13	17	21	25	29	33	38	42	46 47	49	51	53	55	57	59   	61	63	65	66	67	68	69 	
								30	34	39	44	48	50	52	54	56	58	<b>60</b>	62	64						
<b>*</b> 1		6	10	14	18	22	26	31	35																R.	19

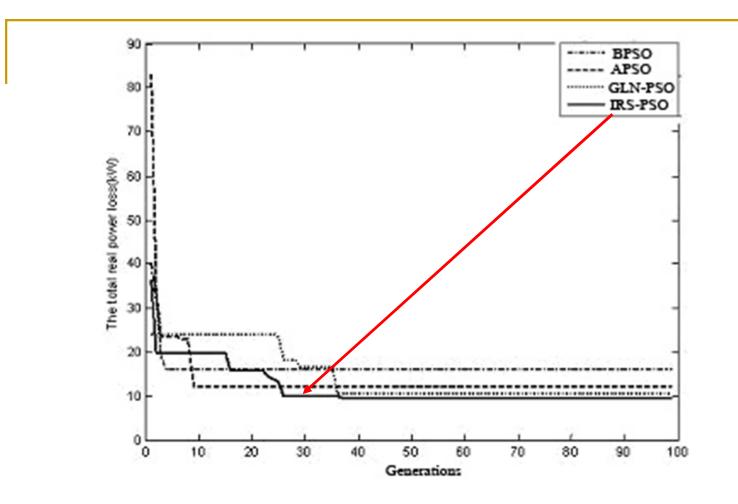
Method		Bus no.	DG		Bus n		DG size		no.		size		Plo			loss	Loss 1	eduction %
			(MW) (	MVAR)		(	MW) (MV	AR)		(MW)	(MVA	R)	(kV	V)	(k'	VAR)	Real	Reactive
		T	e original	power lo	ss in the	69 bus	system						230.1	1962	104	.4490		
IRS-PSO		56		282									23.5	123	14	.6156	89.79	86.01
		56	1.30	356	53		0.5203						7.5	875	8	.3307	96.70	92.02
		56	1.2 1.7 1.2	758	49		0.3529 0.5472 0.3228	1	6		5502 1604		6.3	153	4	.8646	97.25	95.34
	<b>4</b> 7	11 15	5 19 2 	3 27	32 3	6 40	45 									ta		
																1		
	8	12 10		24 28	3	7 41	1								1			
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1 2 3	5 9	13 17	21 2	25 29	33 3	8 42	46 4	9 51 5	3 55	5 57	59	61	63	65	66	67	<mark>68 69</mark>	
ΠБ																		
						43	47											
				30	34 3 	9 44	<b>48</b> 5	0 52 5	4 56	5 58	60	62	64 					
				4								1	1					
	6 10	14 18	22 2	6 31	35													

Method		Type 1	7	Type 2	Type 3		7	Type 4		Ploss (kW)	Qloss (kVAR)
	Bus no.	DG size (MW)	Bus no.	DG size (MVAR)	Bus no.	DG size (MVA)	Bus no.	DG size (MW)	DG size (kVAR)		
				The original po	ower loss ir	the 69 bus s	ystem			230.1962	104.4490
IRS-PSO	56 38 67	1.8281 0.9150 0.1741	56 58 42	1.2992 1.4486 0.4869	56 33	1.5476 0.8735	56	1.5033	1.4313	23.5123 15.0527 9.6187	14.6170 11.0977 8.7658
	4	7 11 1	5 19 2	23 27 32	36 40	45 					
		8 12 1		24 28	37 41						
1 2	3 5	9 13 1	7 21	25 29 33	38 42		51 53	55 57 59	9 61 63	65 66 67	68 69
				30 34	39 44	48 50	52 54	56 58 60	0 62 64		
	6	10 14 1	B 22 2	26 31 35							

MG type	The number of DG (unit)	V <sub>min</sub> (p.u.)	V <sub>avg</sub> (p.u.)	V <sub>max</sub> (p.u.)
The original vo bus system	ltage level in the 69	0.8885	0.9537	0.98
1	3	0.9587	0.9736	0.98
2	3	0.9103	0.9601	0.98
3	3	0.9502	0.9714	0.98
4	3	0.9740	0.9780	0.98
5	4	0.9730	0.9778	0.98

Table VI. The voltage levels in the 69 test system.

Table VI depicts voltage levels of each bus on the 69 bus MG system. In non-DG case, there are voltage levels of some buses which are lower than the low limit (0.90 p.u.). The lowest voltage level is 0.8885 per unit. After DGs are installed, the voltage levels are improved (0.9–0.98 p.u.) which are within the operating range of  $\pm 10\%$ . Note three DGs of MG type 4 and type 5 have little different voltage levels. Furthermore, MG type 4 gives the best average voltage levels compared with other type.



In Figure 4.1, the convergence characteristics of different methods with four different DG types in a MG are shown. IRS-PSO with particle movement converges faster to a better solution than the other methods on the 69 bus MG system.

**Figure 4.1 Convergence characteristics of real power loss minimization when MG has four DG types** 

MG type	Method	1	The 69 bus MG system	m	Standard	
		Ploss <sub>avg</sub> (kW)	Ploss <sub>max</sub> (kW)	Ploss <sub>min</sub> (kW)	deviation	
1	BPSO	73.7267	74.6739	71.2724	1.0239	
	APSO	73.1755	76.0267	70.7626	1.4227	
	GLN-PSO	71.8472	73.3411	70.8859	1.0045	
	<b>IRS-PSO</b>	71.8716	73.3381	70.7626	0.7408	
2	BPSO	150.1792	151.3095	148.3845	0.6786	
	APSO	149.4936	150.1493	148.3845	0.6421	
	<b>GLN-PSO</b>	149.4824	150.7666	148.3845	0.7454	
	IRS-PSO	149.1244	150.1148	148.3845	0.4620	
3	BPSO	93.6108	94.9339	91.6334	0.7874	
	APSO	92.7820	94.8750	91.5170	1.0124	
	<b>GLN-PSO</b>	93.1101	94.9098	91.5171	1.0476	
	<b>IRS-PSO</b>	92.4182	94.2841	91.5060	1.0007	
4	BPSO	14.2072	17.9239	15.3254	2.1239	
	APSO	12.5498	16.5498	11.2669	3.3927	
	GLN-PSO	11.1973	17.4145	8.0046	2.0272	
	IRS-PSO	9.3895	12.3519	6.3153	1.5864	
5	BPSO	24.9358	31.9157	25.4921	4.2728	
	APSO	16.8993	21.2939	16.7280	2.2988	
	GLN-PSO	18.4923	21.4473	16.1829	2.4222	
	<b>IRS-PSO</b>	15.9841	20.9372	15.0527	2.2892	

Table VII. The statistic variances of BPSO, APSO, GLN-PSO, and IRS-PSO for Optimal three DGs placement.

Table 7 shows that the average and minimum real power losses of IRS-PSO are lessthan the other methods for every MG types on the 69 bus system with smallerstandard deviations.

# **5.** Conclusion

In this research, IRS-PSO method effectively determines the optimal placement of distributed generation in a microgrid.

The salient features include four vectors of particle movement, resulting in a better search direction than BPSO and APSO. Moreover, IRS-PSO can escape from the local optimum by reinitiaization process.

Test results indicate that IRS-PSO with MG type 5 in microgrid renders the minimum loss in a faster convergence rate than BPSO, APSO, and GLN-PSO on the 69 MG distribution system.