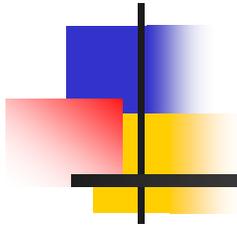




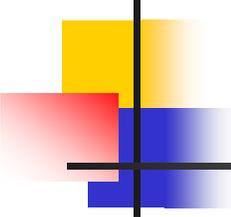
PQSynergy 2014 19 May 2014



Modeling and Control of Photovoltaic Grid
Connected Inverter Based on Nonlinear System
Identification for Power Quality Analysis



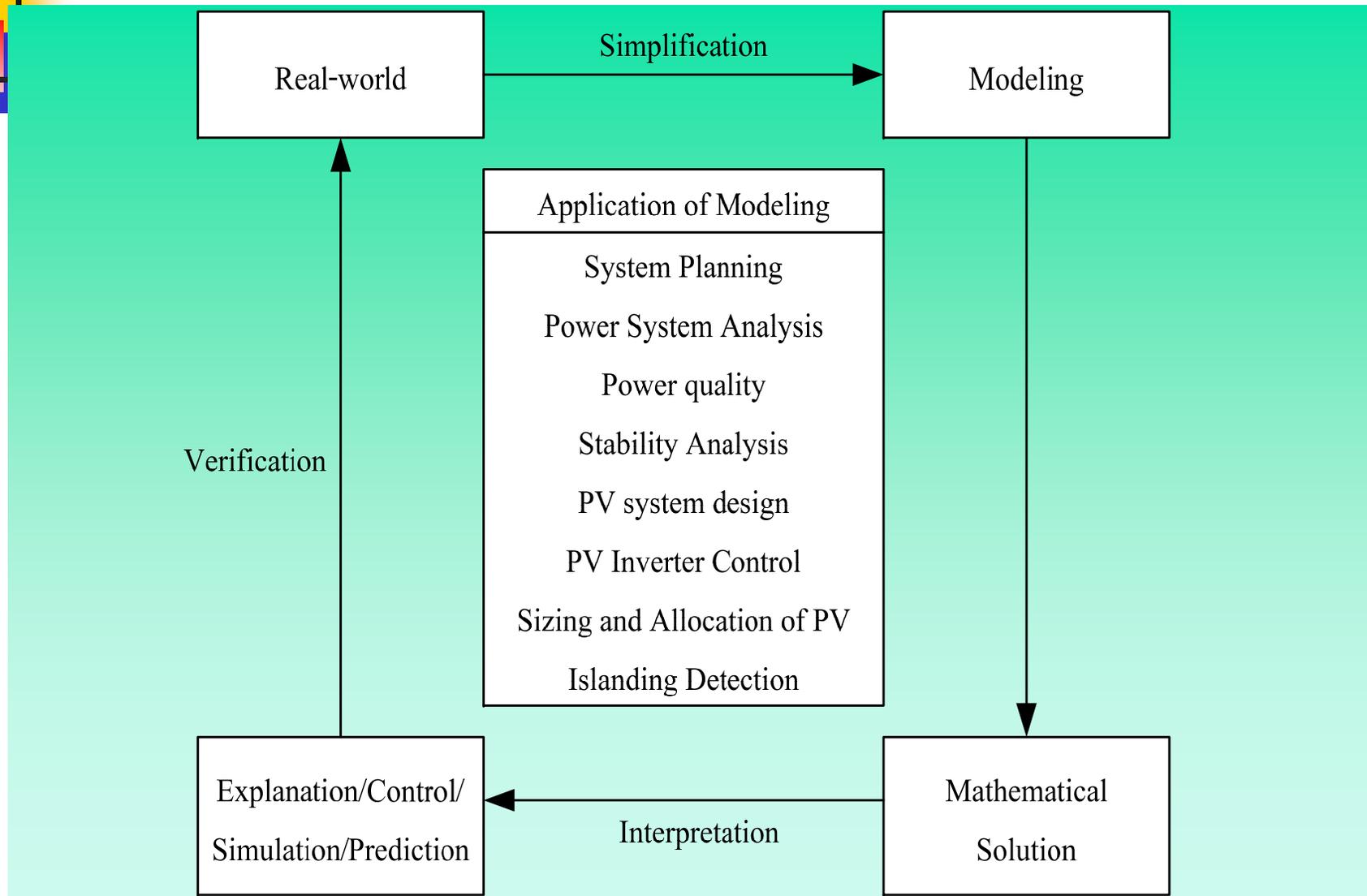
Dr. Nopporn Patcharaprakiti
Rajamangala University of Technology Lanna Chiangrai
19 May 2014



TOPIC

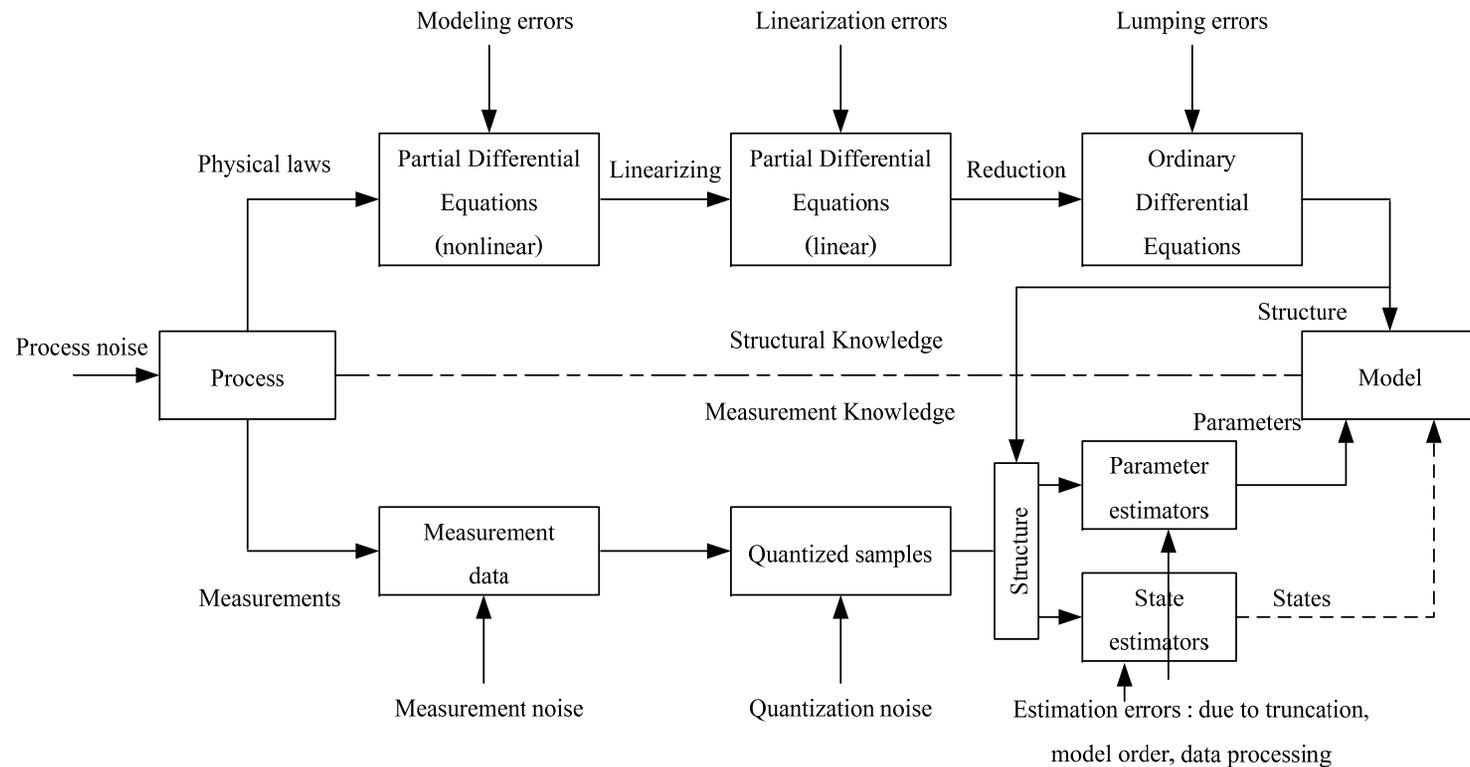
- **INTRODUCTION**
- **MATHEMATICAL MODELING**
- **NONLINEAR SYSTEM IDENTIFICATION**
- **CASE STUDY WITH PV INVERTER**
- **POWER QUALITY ANALYSIS**
- **MODELING APPLICATION**
- **CONCLUSION**

Mathematical Modeling of system

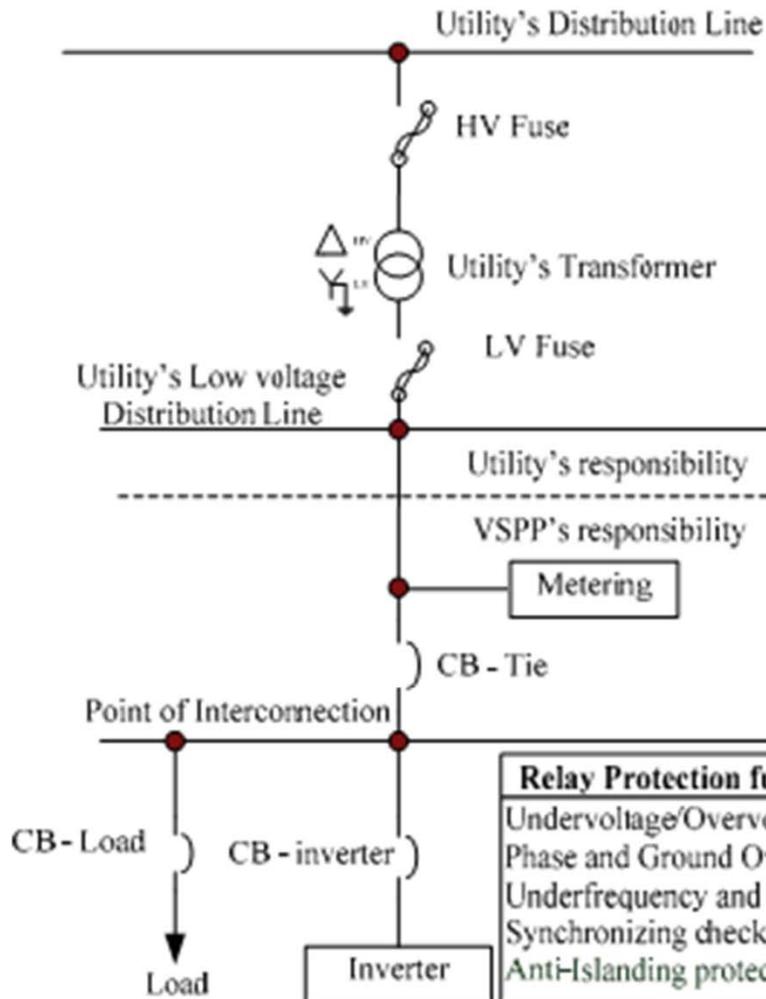


Method for system Modeling

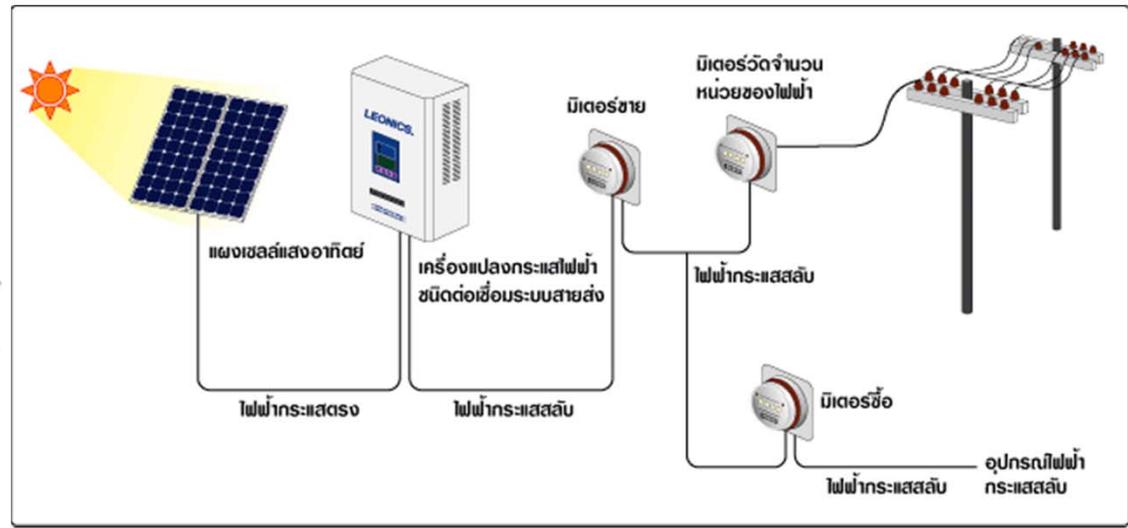
- Analytical (Theory & Circuit)
- Experimental (System Identification)



Grid connected Inverter of PV

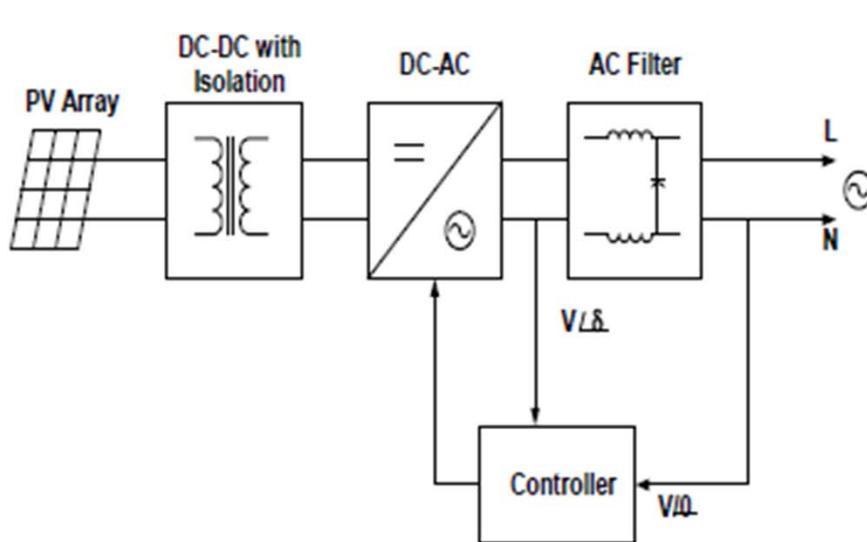


Relay Protection function of Inverter
Undervoltage/Overvoltage (27/59)
Phase and Ground Overcurrent (50/51)
Underfrequency and Overfrequency (81)
Synchronizing check (25)
Anti-Islanding protection

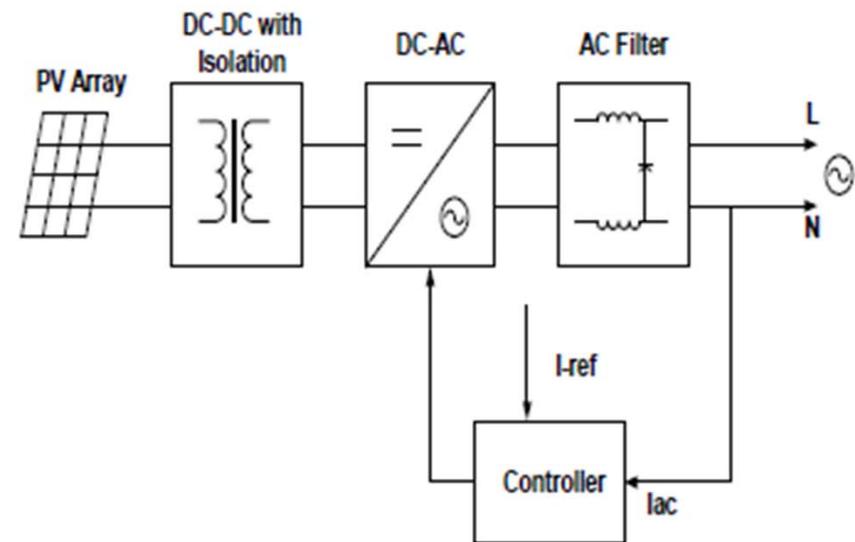


Inverter Configuration

■ Voltage source Inverter

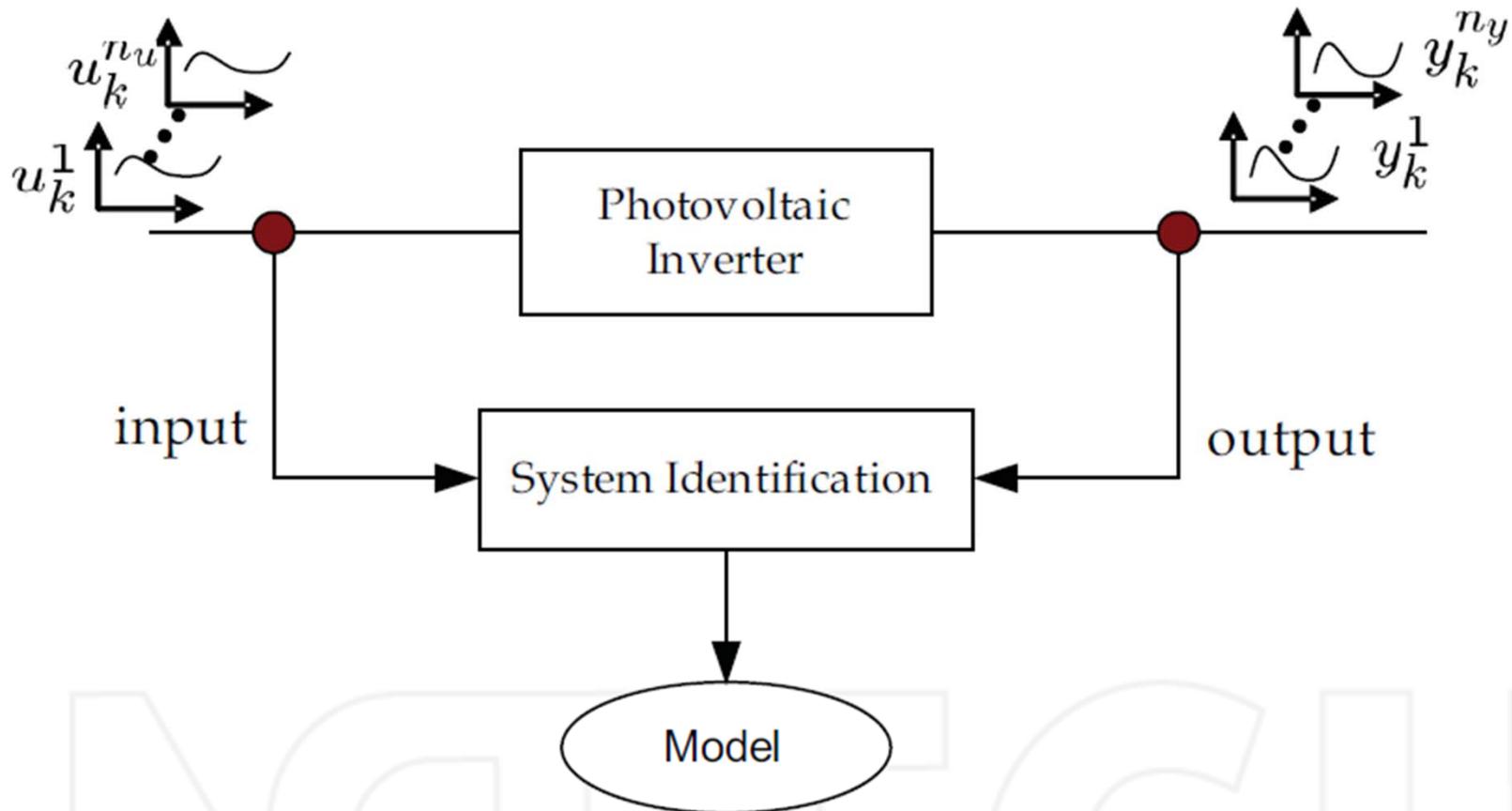


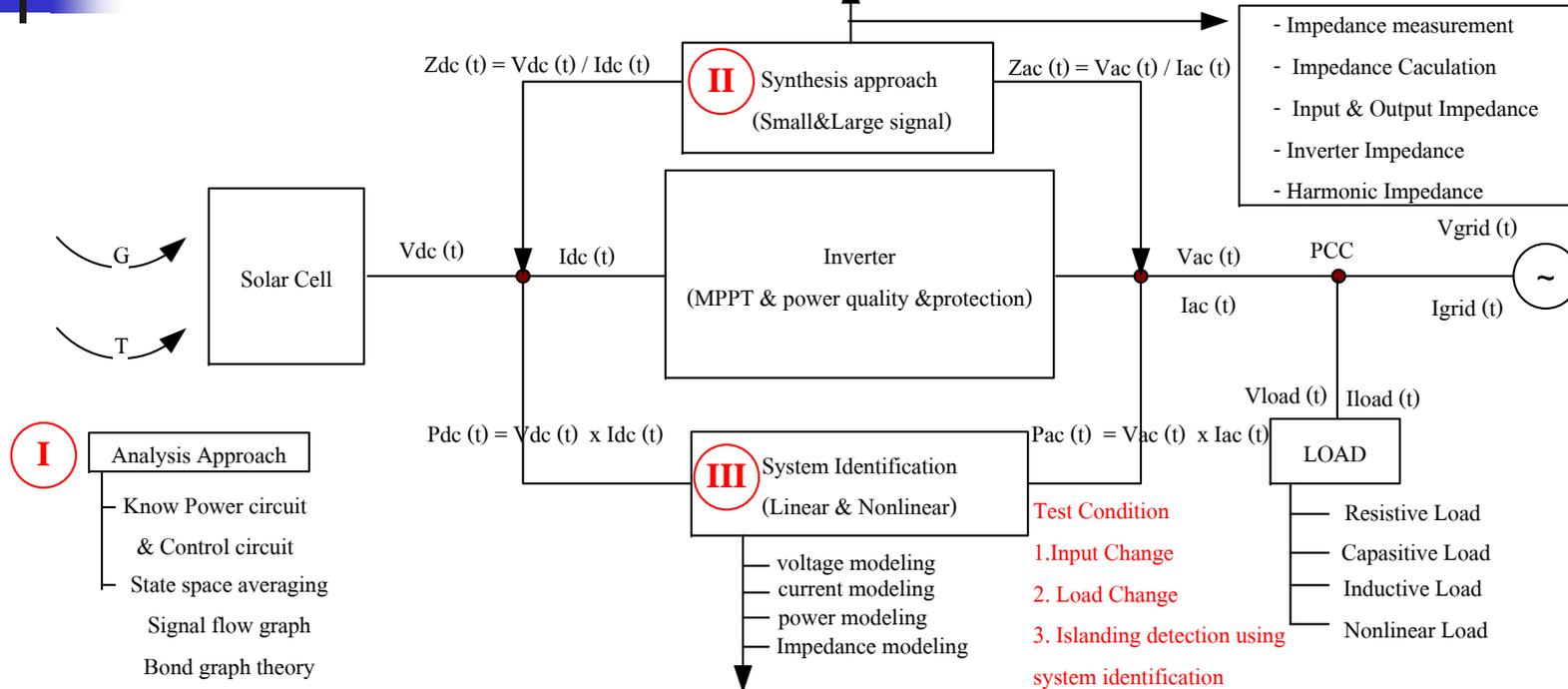
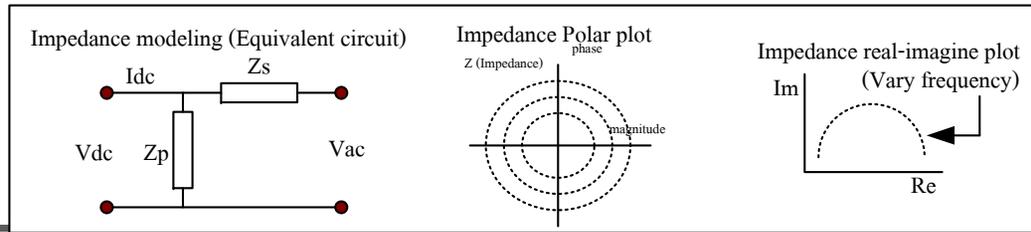
(a) Voltage Control Inverter



(b) Current Control Inverter

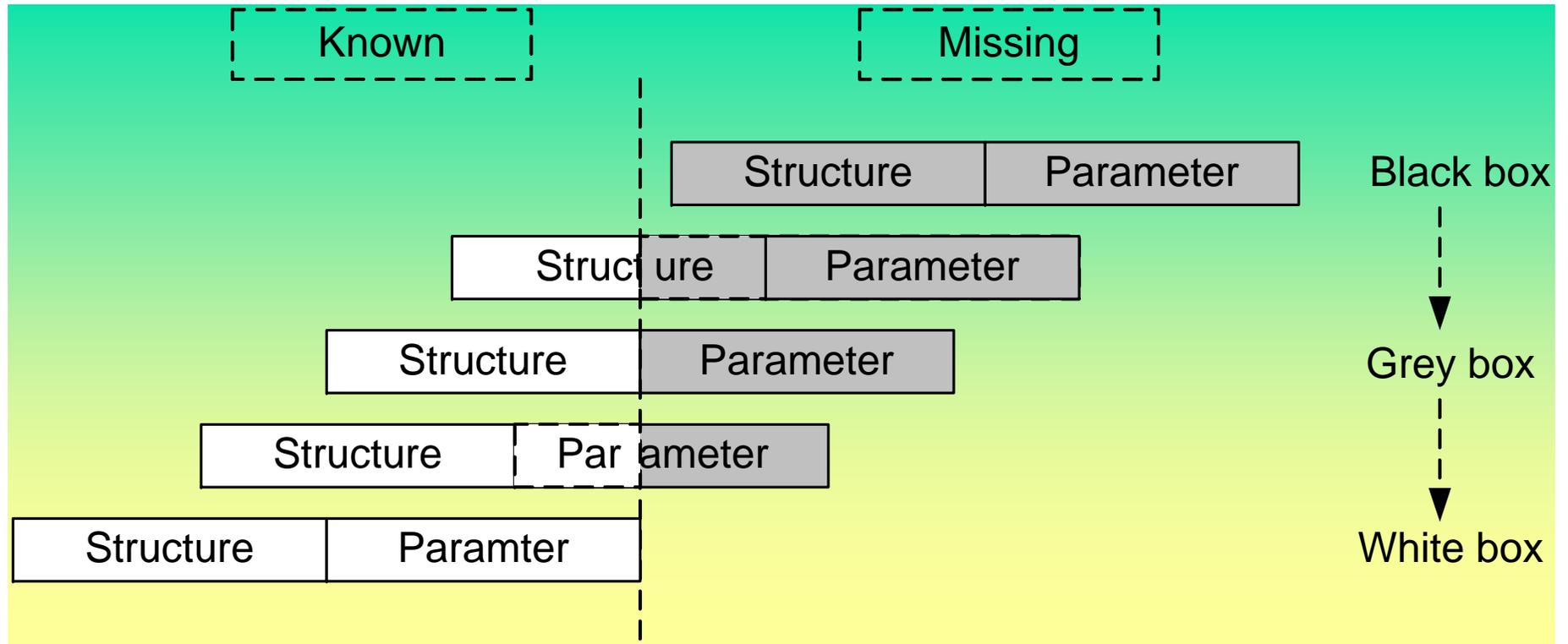
PV Inverter



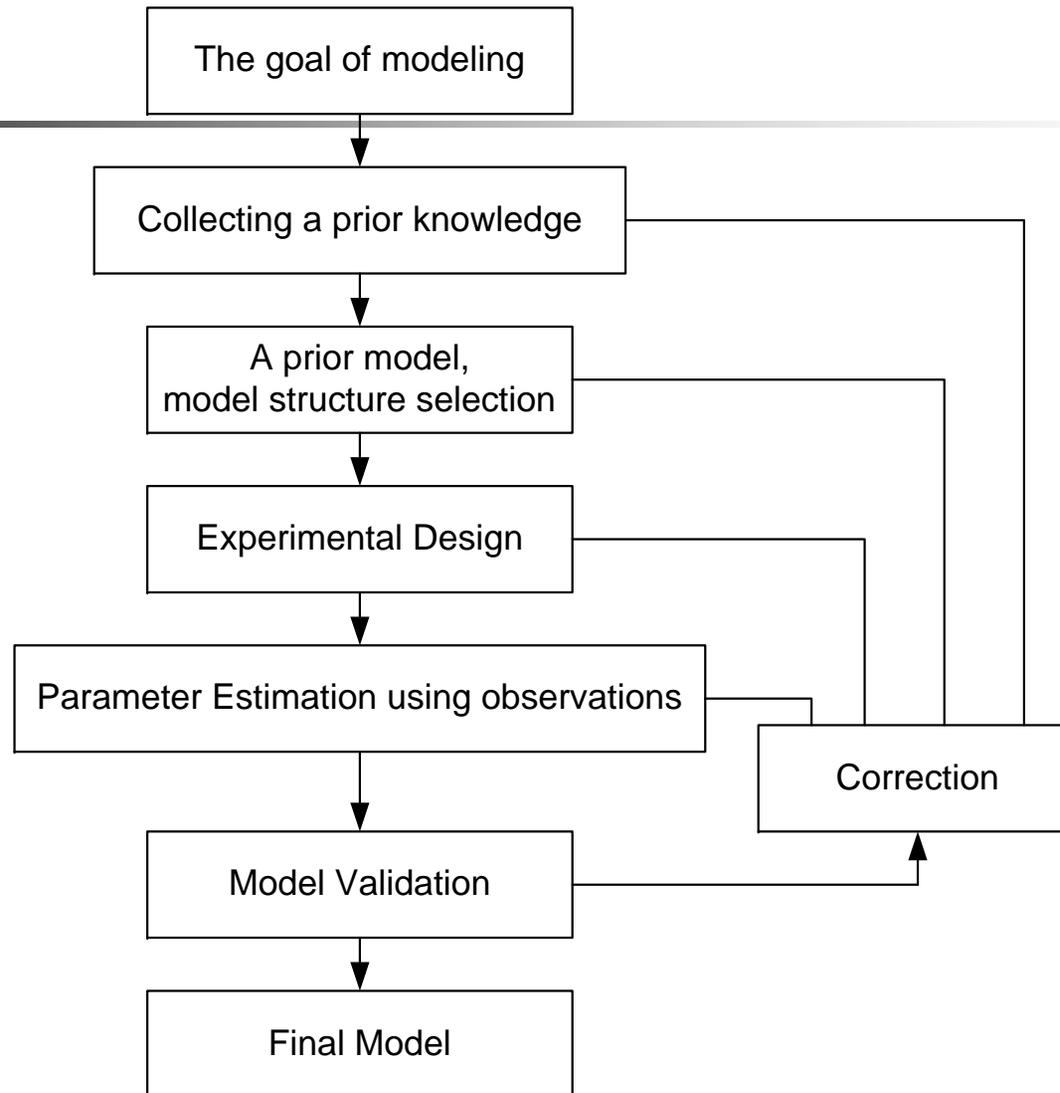


Linear Tool Analysis	Simulation and Prediction	Mathematical Equation	Nonlinear Analysis
		$x(t + Ts) = Ax(t) + Bu(t) + Ke(t)$ $y(t) = Cx(t) + Du(t) + e(t)$ $y(t) = \begin{bmatrix} B(q) \\ F(q) \end{bmatrix} u(t) + e(t)$	<ul style="list-style-type: none"> - Function Analysis - Chaos - Bifurcation - Irreversibility

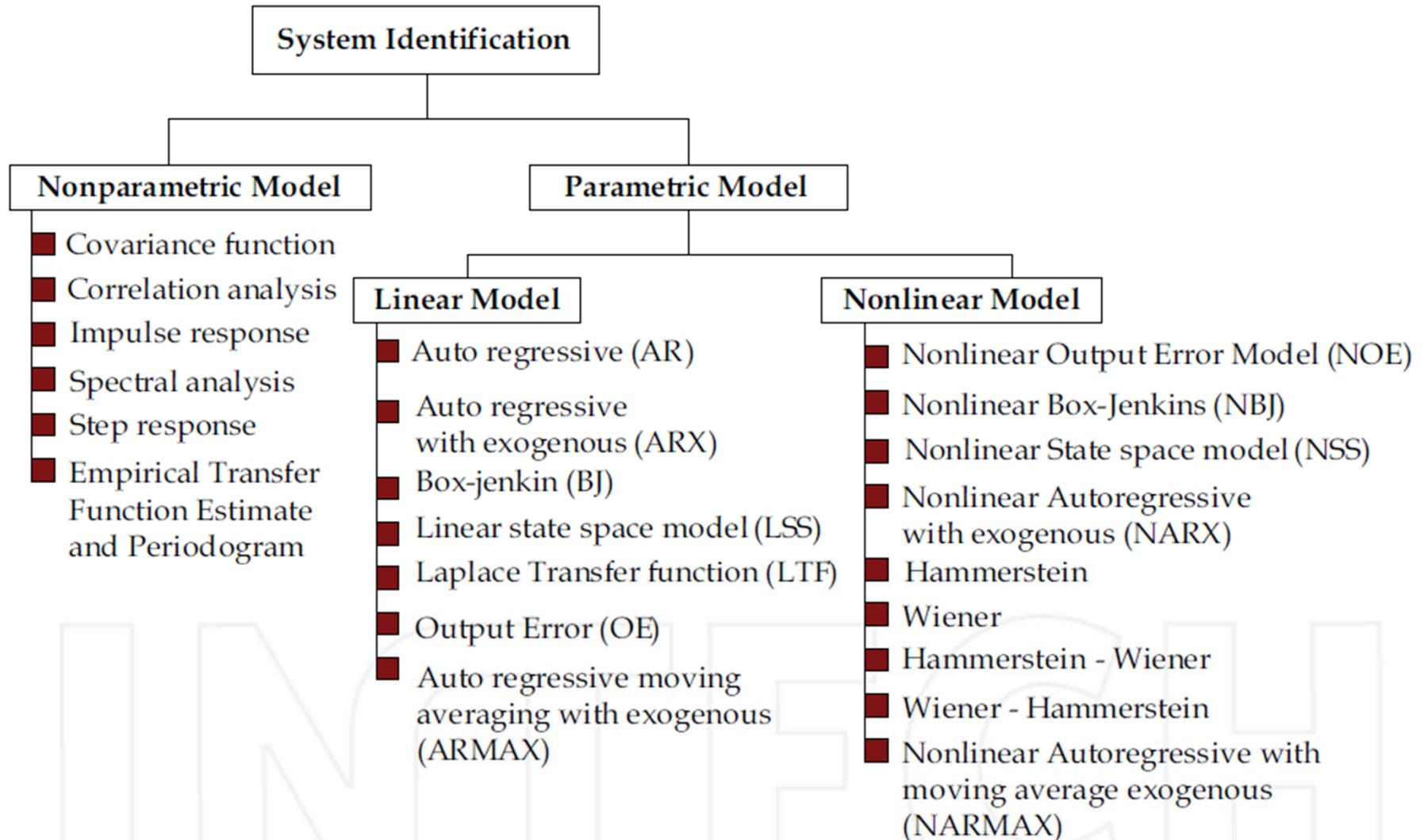
Principle of System



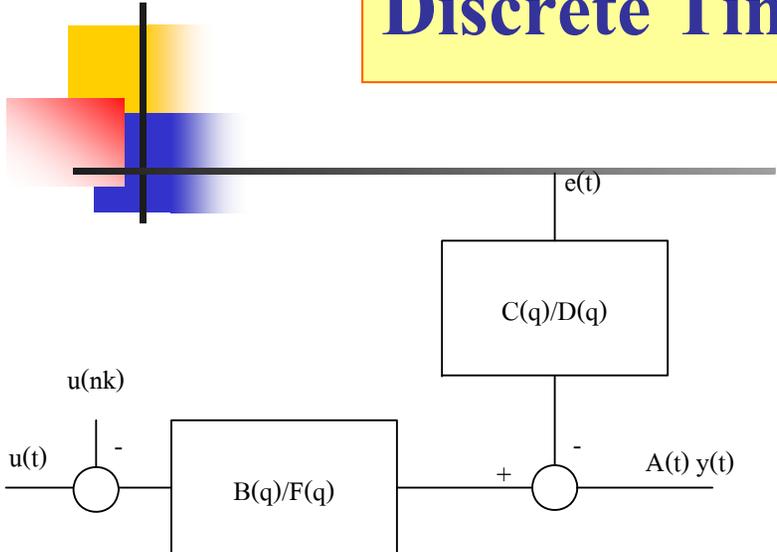
System Identification



Type of System Identification



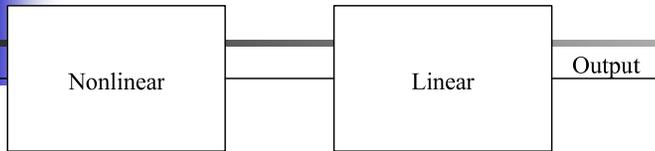
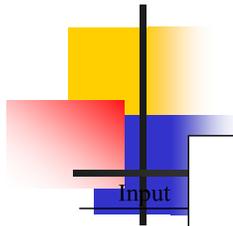
Discrete Time Linear Model



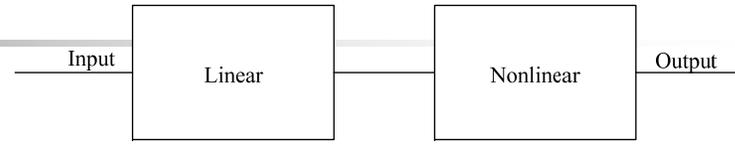
Model Structure	Discrete Time Form
ARX	$A(q)y(t) = \sum_{i=1}^{nu} B_i(q)u_i(t - nk_i) + e(t)$
ARMAX	$A(q)y(t) = \sum_{i=1}^{nu} B_i(q)u_i(t - nk_i) + C(q)e(t)$
Box-Jenkins (BJ)	$y(t) = \sum_{i=1}^{nu} \frac{B_i(q)}{F_i(q)} u_i(t - nk_i) + \frac{C(q)}{D(q)} e(t)$
Output Error (OE)	$y(t) = \sum_{i=1}^{nu} \frac{B_i(q)}{F_i(q)} u_i(t - nk_i) + e(t)$

- $u(t)$ – input
- $y(t)$ – output
- $e(t)$ - error
- $A(q), B(q), C(q), D(q), E(q)$ – Coefficient
- q –shift operator

Nonlinear System Identification



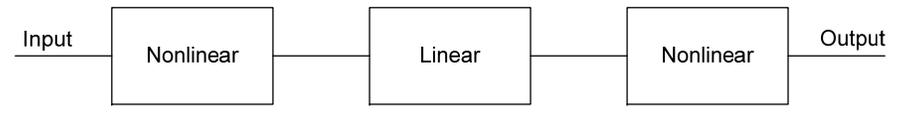
Hammerstein Model



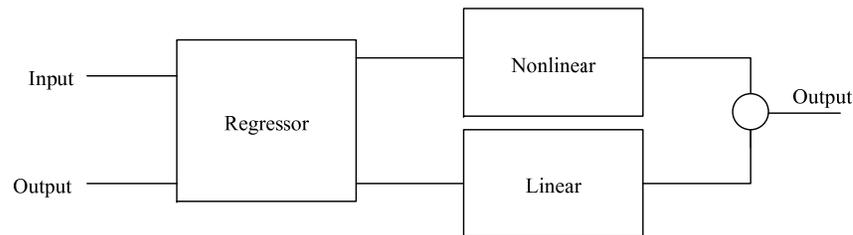
Weiner Model



Weiner-Hammerstein Model

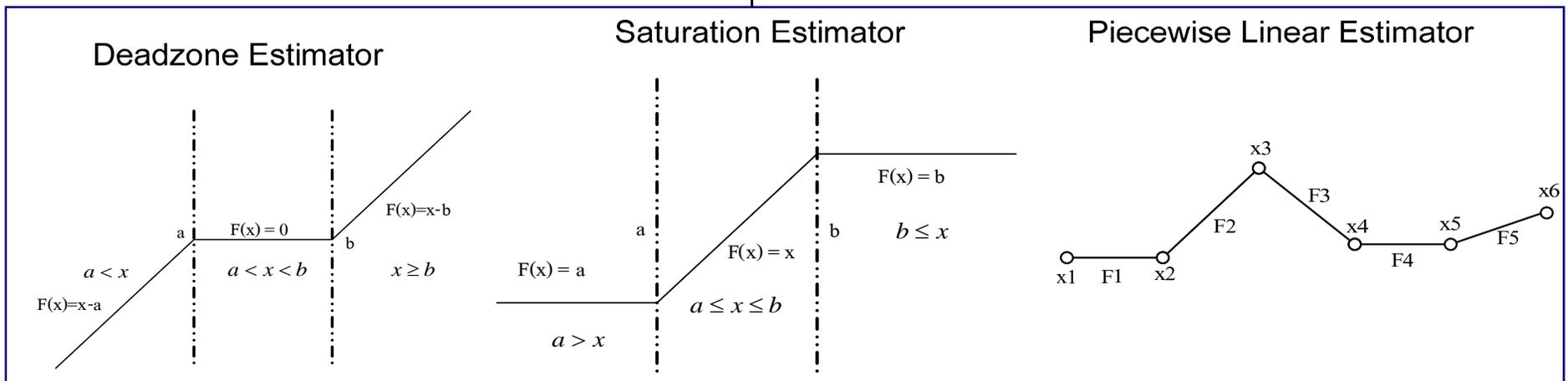
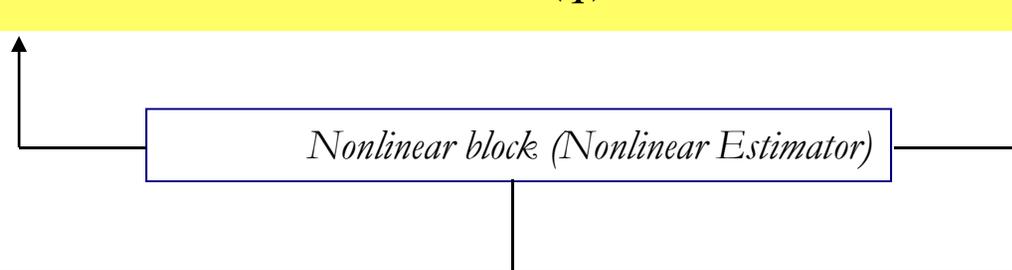
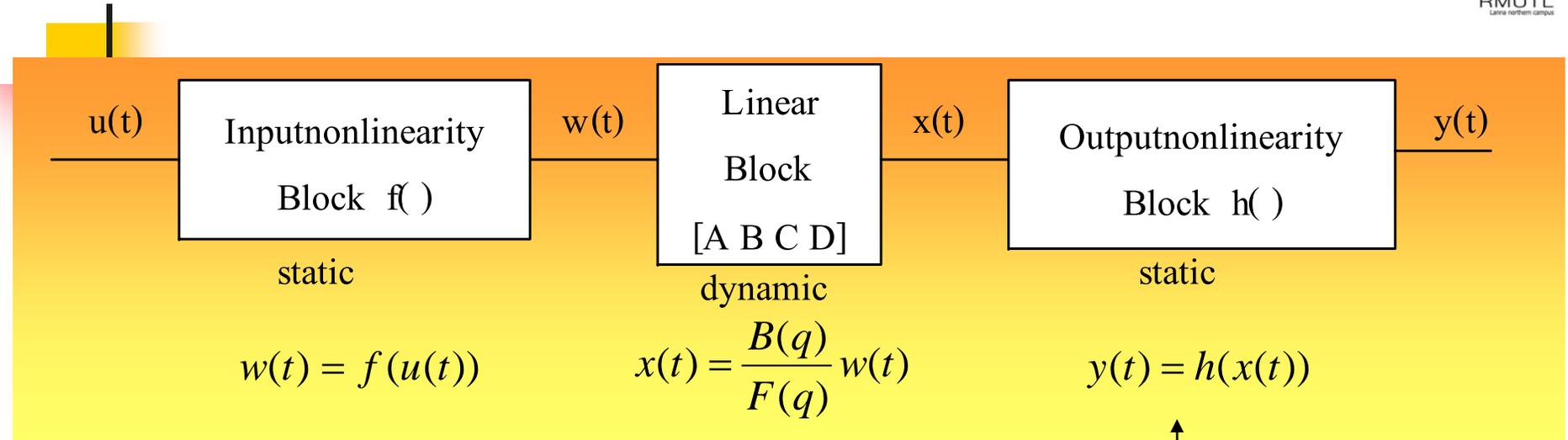


Hammerstein-Weiner Model



Nonlinear Auto Regressive with exogenous Model

Structure of Hammerstein-Weiner Model



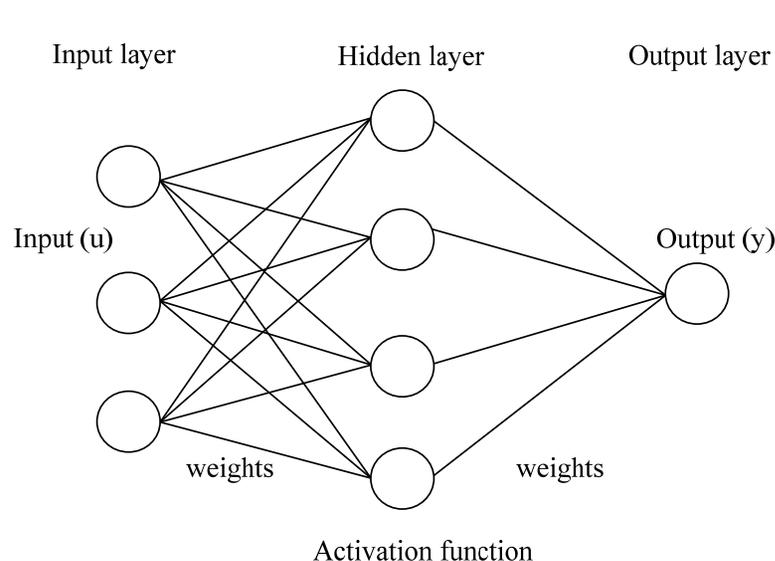
Nonlinear block (Nonlinear Estimator)

Wavelet Network (Wavenet Nonlinear Estimator : WN) ❖

Wavelet Transform

$$y = (u - r)PL + \sum_i^n as_i * f(bs(u - r)Q + cs) + \sum_i^n aw_i * g(bw_i(u - r)Q + cw_i) + d$$

Neural Network (Sigmoid Network : SN)



$$y(u) = (u - r)PL + \sum_i^n a_i f((u - r)Qb_i - c_i) + d$$

Criteria for Model Selection

Accuracy

$$fit = 100 * (1 - norm(y^* - y) / norm(y - \bar{y}))$$

highest

Final Prediction Error

$$FPE = V \begin{pmatrix} 1 + \frac{d}{N} \\ 1 - \frac{d}{N} \end{pmatrix}$$

smallest

Loss Function

$$V = \det \left(\frac{1}{N} \sum_1^N \varepsilon(t, \theta_N) (\varepsilon(t, \theta_N))^T \right)$$

highest •

Akaike's Information Criteria

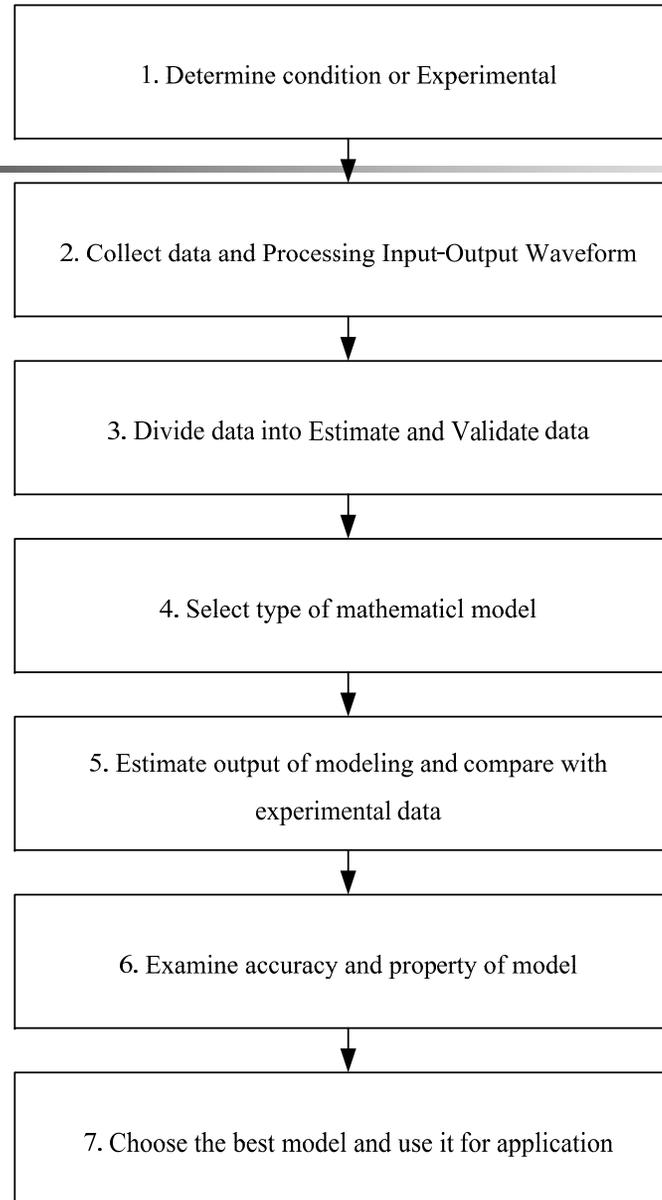
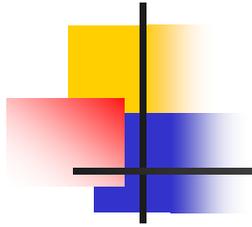
$$AIC = \log V + \frac{2d}{N}$$

smallest

lowest order

number of pole (nb) plus zero (nf) order calculate •

Research Methodology



Testing inverter

Frobus IG 1500 W

Leonics Apollo G300 5000 W

LEONICS

APOLLO G-300

GRID CONNECTED INVERTER



Wall mount case

- Pure sine wave power output
- Peak efficiency > 91% (include isolation transformer)
- Low Harmonic Distortion (THDi) less than 4%
- Main and solar generator are galvanically isolated
- Built-in Maximum Power Point Tracking (MPPT)
- Microprocessor control
- Advanced IGBT Technology
- Islanding protections during failure of utility grid power supply
- Fully automatic self-START in the morning and

LEONICS

APOLLO G-300 series GRID CONNECTED INVERTER



MODEL	Wall Mount type	G-303	G-304	G-304M2	G-305	
	Rack Mount type*	G-303RM	G-304RM	G-304M2RM	G-305RM	
RATED POWER	PV input	2.8 kWp	3.9 kWp	4.7 kWp	5.8 kWp	
	AC output	2.5 kW	3.5 kW	4.2 kW	5 kW	
SYSTEM	Controller Technology	Intelligent with microcomputer controlled IGBT technology				
DC INPUT	Operating voltage range	85 - 300 V				
	Max. admissible voltage (for short period time)	350 V				
GRID LINE	Voltage and phase	±10% / -1% for 230 Vac and 230 Vac (single phase) according to standards of IEC 61727 and IEC 62118 200 - 250 Vac for 240 Vac (single phase) according to standards of AS 4777 200 - 240 Vac for 230 Vac (single phase) according to standards of IEC 61727 and IEC 62118 (for PEA grid line) 200 - 240 Vac for 230 Vac (single phase) according to standards of IEC 61727 and IEC 62118 (for MEA grid line)				
	Frequency	50 / 60 Hz and 50 Hz for 230 Vac and 230 Vac 50 / 60 Hz ± 0.6 Hz for 240 Vac				
AC OUTPUT	Power factor	48 - 61 Hz for 230 Vac and 230 Vac according to standards of IEC 61727 and IEC 62118 (for PEA and MEA grid line)				
	Total harmonic distortion	Total harmonic distortion 4% max. 4.8% max. 3%				
	Current limiting	100%				
SOLUTION EFFICIENCY	Operating efficiency	91%				
CONTROL PROTECTION	Peak efficiency	91%				
	Input / Output	Automatic cooling fan / MPPT control / Anti-power diode control				
	Islanding	Over voltage / Under voltage / AC & DC / Frequency (AC)				
	Over heat	Voltage and phase anti detection				
	Surge energy of capacitor	Auto shut-down and auto restart				
	LED	285 Joules / 10 / 1,000 impulses max. form				
INDICATOR	LCD display	Main, Operating, Alarm				
	ADJ. ALARM	DC / AC voltage, Current, Watt, Today kWh, Accumulated kWh, Calendar, Clock, Condition setting, Fault				
	COMMUNICATION	Multi-tone sound with reset for silence				
	INTERFACE	RS-232 serial interface port				
	ACOUSTIC NOISE	RS-485 interface				
	ENVIRONMENT	At 1 m distance				
	TEMPERATURE	within 50 dBA				
	HUMIDITY	0 - 45°C				
DIMENSION	Wall mount case	37.5 x 45 x 22.9	37.5 x 45 x 22.9	43.9 x 52 x 28	43.9 x 52 x 28	
	Rack mount case	48.2 x 19.8 x 47	48.2 x 19.8 x 47	48.2 x 22 x 40.7	48.2 x 22 x 40.7	
WEIGHT	Wall mount case	24	24	31	31	
	Rack mount case	23	23	28	28	
DESIGN RESOLUTION	Rated according to	AS 4777, AS 3100, IEC 61727 and IEC 62118				

*The maximum voltage mentioned in the table is the maximum continuous voltage for the inverter. The maximum voltage for the inverter is the maximum voltage for the inverter. The maximum voltage for the inverter is the maximum voltage for the inverter.

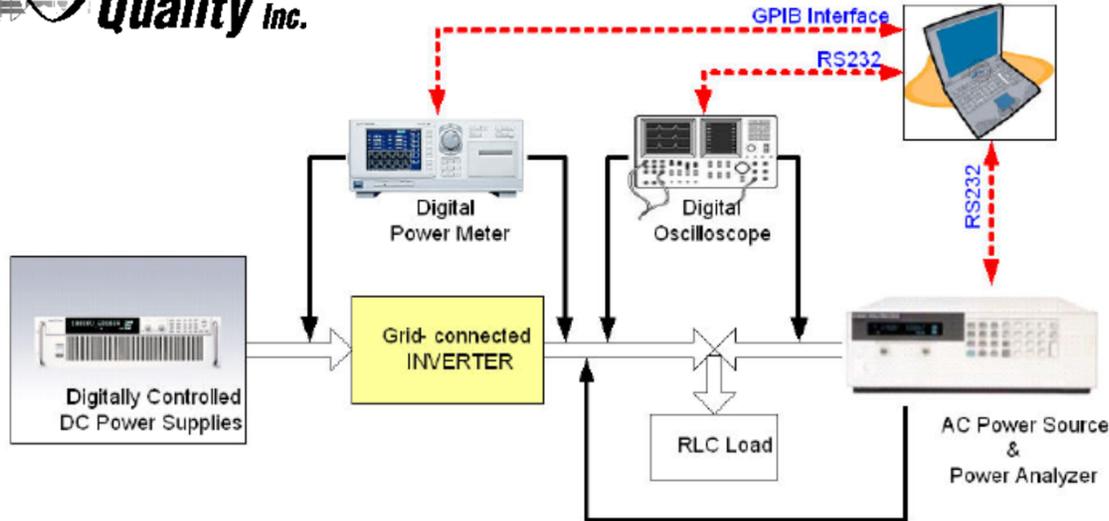
Authorized Dealer
LEO ELECTRONICS CO., LTD.
27, 20 Soi Bangna-Trad Rd. 31, Bangna, Bangkok 10260 THAILAND
Tel: 0-2748-2000, 0-2748-8708 Fax: 0-2748-8712 e-mail: PVE@leo-electronics.com
www.leonics.com

Authorized Dealer

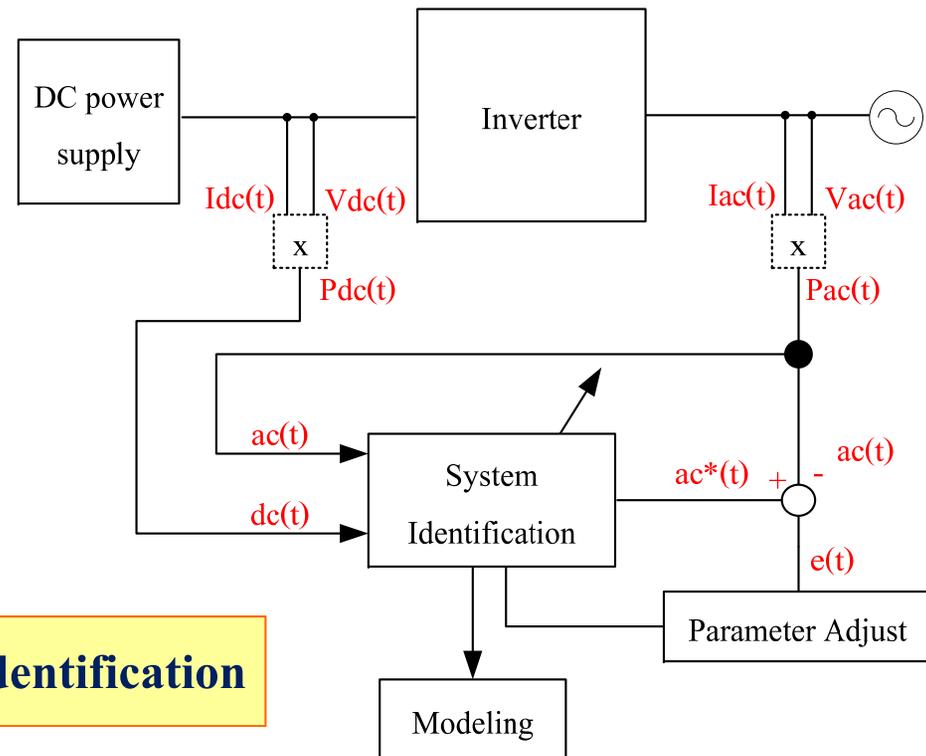
TECHNICAL DETAILS.

It goes without saying that every FRONIUS IG complies with all the obligatory guidelines and standards of each country. More in-depth information and certificates may be viewed at www.fronius.com under "downloads". Of course, all FRONIUS IG bear the CE mark.

TECHNICAL DATA	FRONIUS IG 15	20	30	40	60 HV
MPP voltage range	150 - 400 V	150 - 400 V	150 - 400 V	150 - 400 V	150 - 400 V
Max. input voltage (at 1000 W/m ² ; -10°C)	500 V	500 V	500 V	500 V	530 V
PV array output	1300 - 2000 Wp	1800 - 2700 Wp	2500 - 3600 Wp	3500 - 5500 Wp	4600 - 6700 Wp
Nominal output	1300 W	1800 W	2500 W	3500 W	4600 W
Max. power output	1500 W	2000 W	2650 W	4100 W	5000 W
Max. efficiency	94.2 %	94.3 %	94.3 %	94.3 %	94.3 %
Euro efficiency	91.4 %	92.3 %	92.7 %	93.5 %	93.5 %
Mains voltage/frequency	230 V / 50 Hz (60 Hz)				
Size (l x w x h)	368 x 344 x 220 mm (500 x 435 x 225 mm) 610 x 344 x 220 mm (733 x 435 x 225 mm)				
Weight	9 kg (12 kg)		16 kg (20 kg)		
Cooling	controlled forced-air cooling				
Housing variations	designer internal housing; optional outer housing				
Ambient temperature range	+20 50 °C				

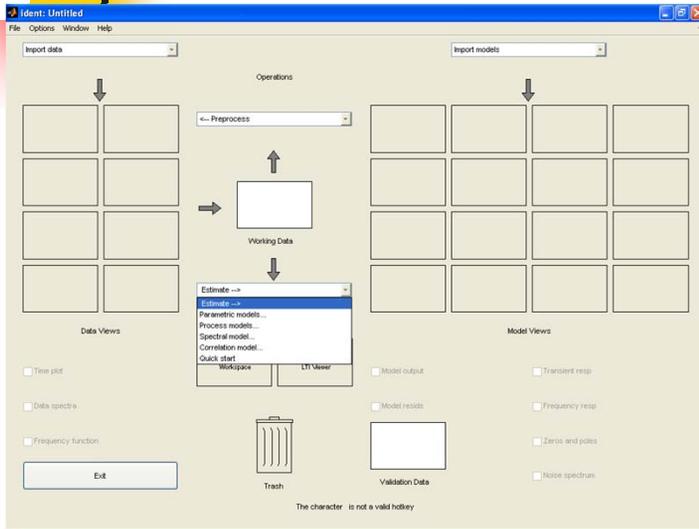


Experimental setup

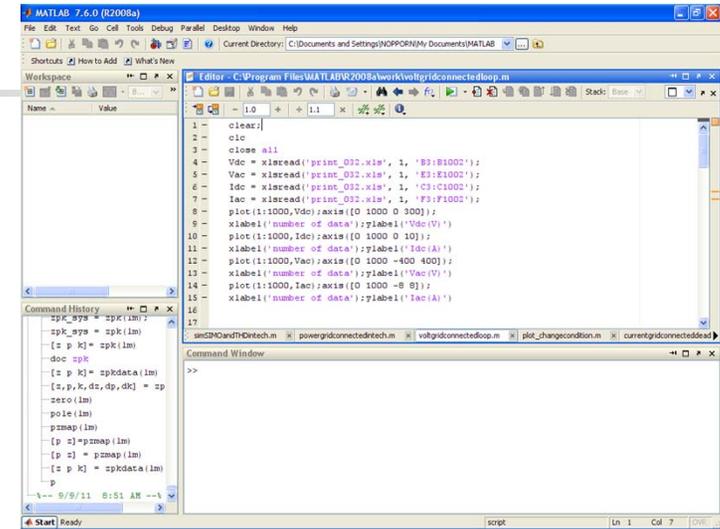


inverter modeling using system identification

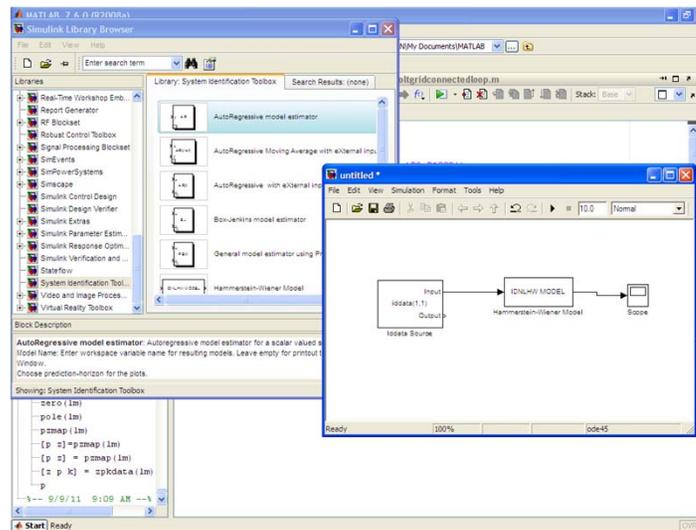
Using System Identification Toolbox in MATLAB



Toolbox



M-file

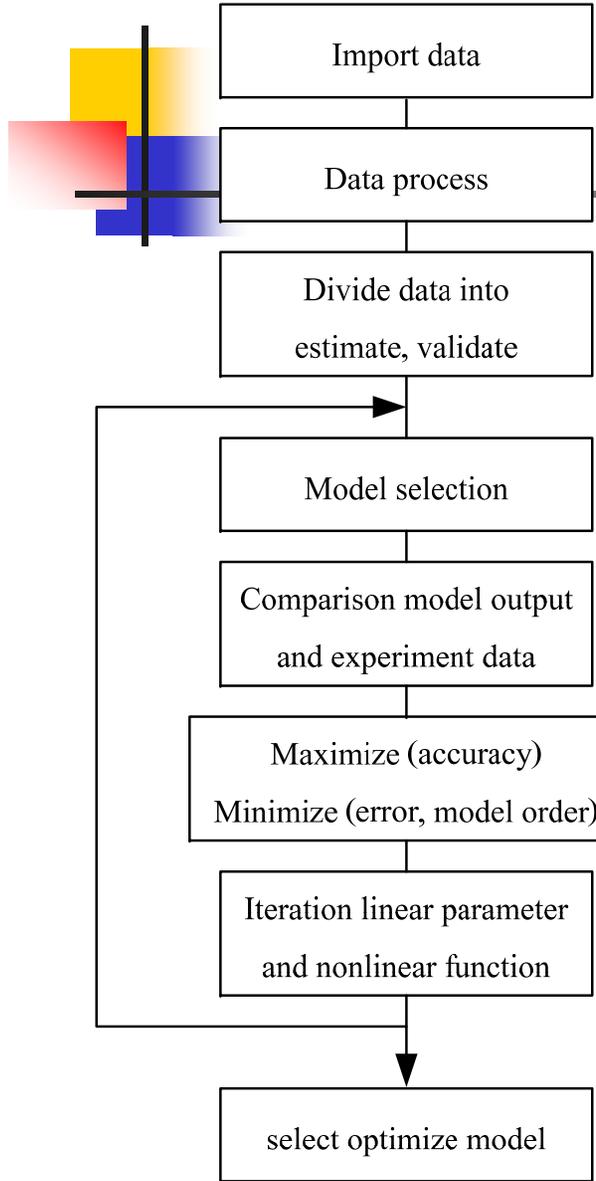


simulink

Flow chart

คำสั่งที่ใช้

Write M-file



Xlsread (....)

Resampling(...)
IDDATA(...)

Identify (number)

oe(...)
nlhw (...)

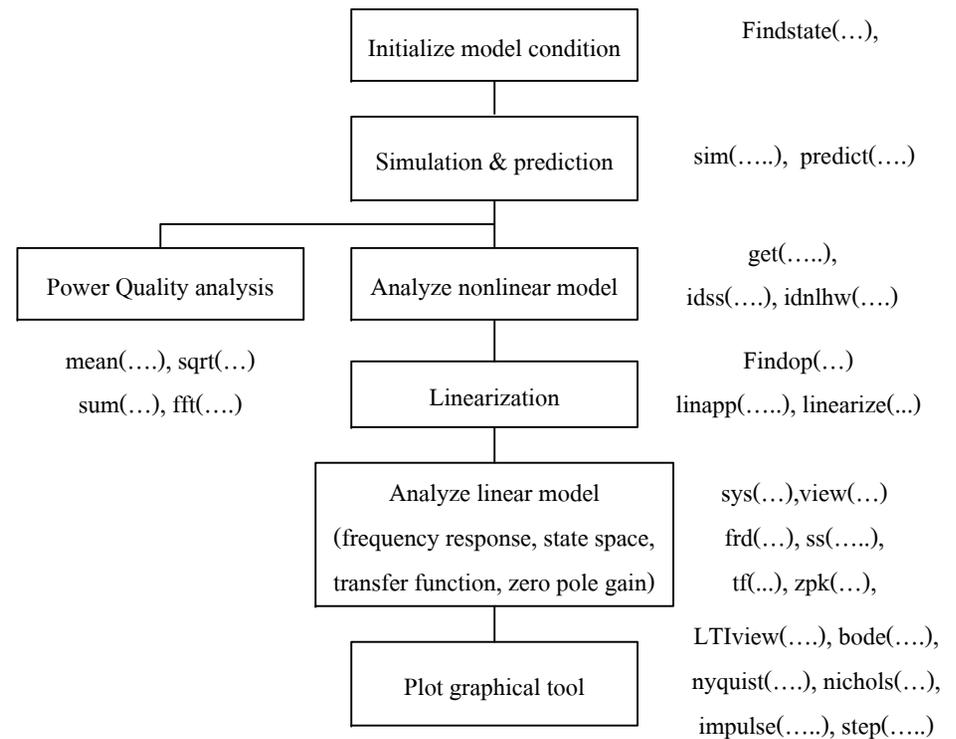
Compare(...)

If loop
max(), min()

For loop

System Modeling

Modeling Analysis

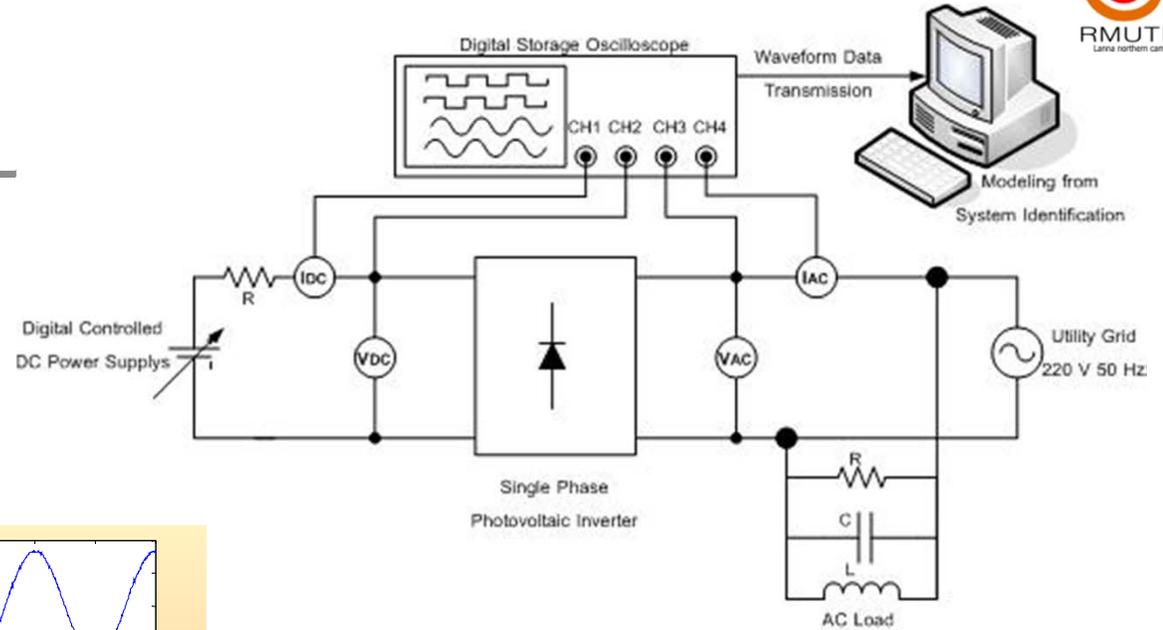
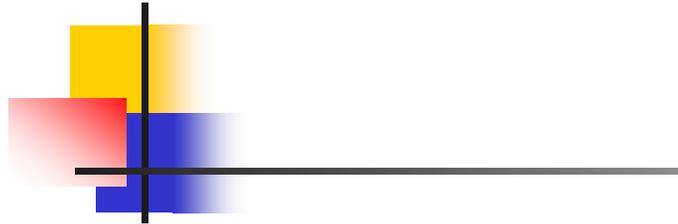


- **Modeling System in Steady state**
- Modeling System in Transient
- Modeling System in Islanding
- Modeling System with cross validation
- Modeling with MIMO model

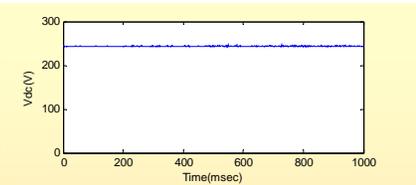
Modeling and Condition from Experimental

Type of Modeling	Parameter	Condition
Linear Modeling		
Auto Regressive with Exogenous,	SISO	Steady state
Auto Regressive Moving Average with Exogenous	SISO	Steady state
Box-Jenkins (BJ)	SISO	Steady state
Output error (OE)	SISO	Steady state
Nonlinear Modeling		
Nonlinear Autoregressive with Exogenous	SISO	Steady state
Hammerstein	SISO	Steady state
Wiener	SISO	Steady state
Hammerstein-Wiener	SISO	Steady state

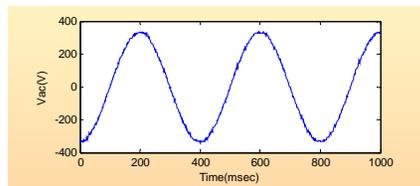
Experimental in Steady State



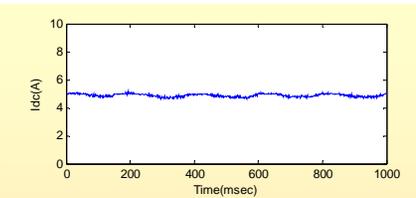
Input and Output waveform



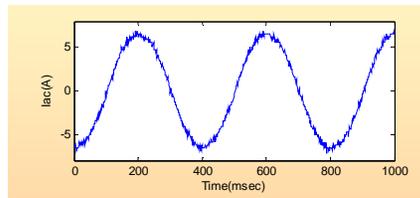
DC Voltage



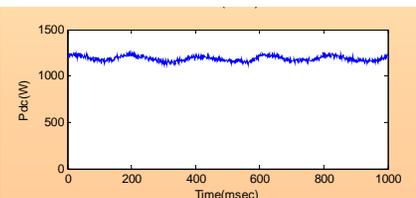
AC Voltage



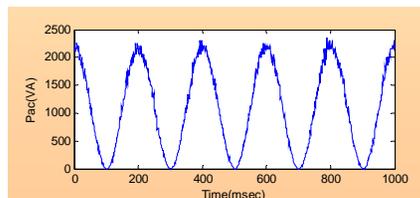
DC Current



AC Current



DC Power

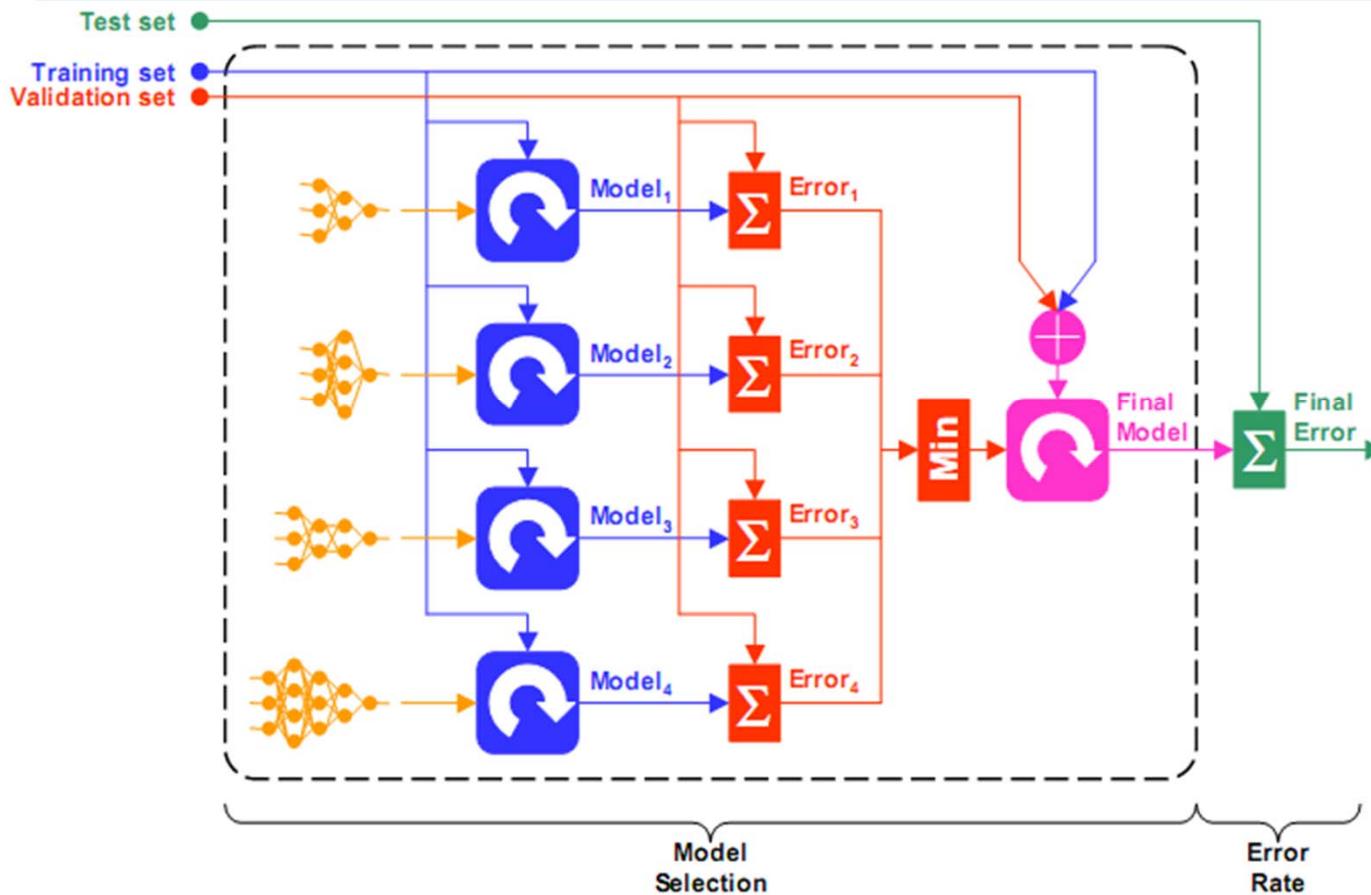


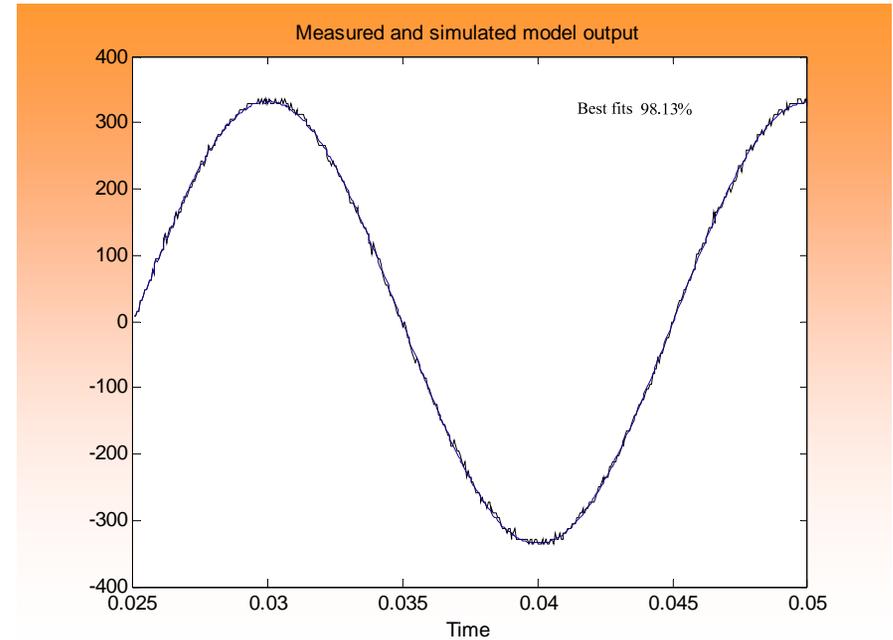
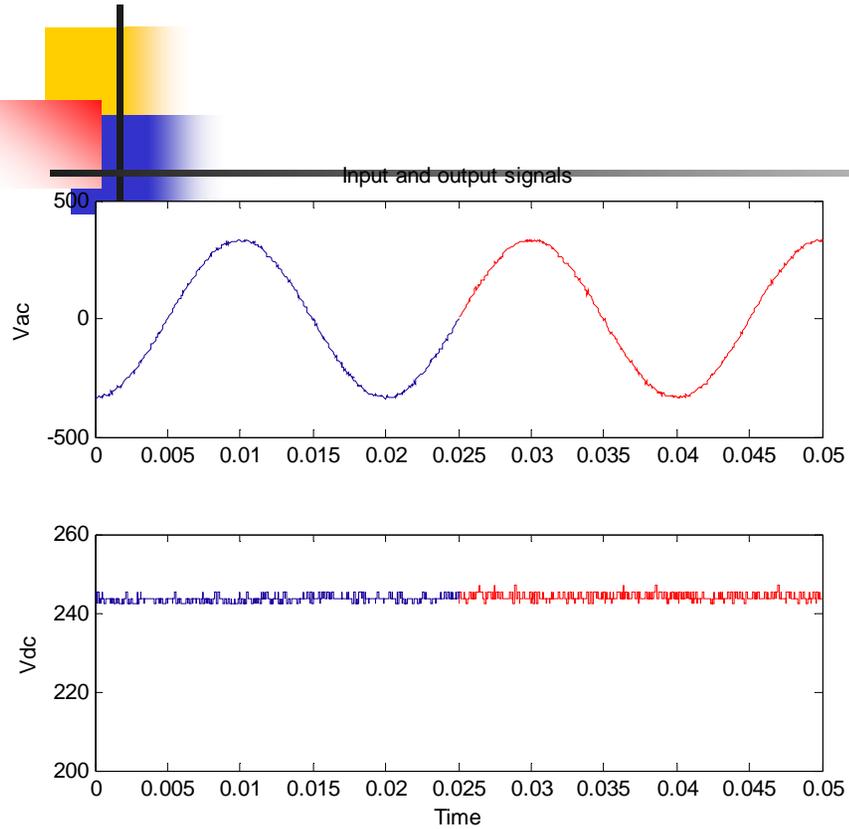
AC Power

Experimental Setup

Three Way Data Splits

Three-way data splits





Data divide into estimate and validate data

The experiment and simulated model output

Result of Modeling

Model	Linear Polynomial Parameters						% fit	FPE	AIC
	a_n	b_n	c_n	d_n	f_n	k_n			
Arx	10	10	-	-	-	9	26.49	3,292	8.09
Armax	5	1	3	-	-	3	92.03	2,584	7.85
BJ	-	5	5	1	3	1	92.82	2,655	7.88
OE	-	3	-	-	3	5	93.56	2,910	7.97

Model	Nonlinear		Linear			Model properties		
			a_n	b_n	k_n	% fit	FPE	AIC
NARX	-	WN	9	1	9	81.02	5,012	8.51
	-	SN	10	7	8	81.01	4,086	8.30
Model	Nonlinear		Linear			Model properties		
	I/P	O/P	b_n	f_n	k_n	% fit	FPE	AIC
Hammerstein	SN	-	3	3	1	92.79	4,022	9.54
	WN	-	3	3	1	92.88	3,037	9.47
Wiener	-	SN	2	5	0	53.86	3,790	11.86
	-	WN	4	2	2	61.03	3,013	10.28
Hammerstein-Wiener	SN	SN	4	2	2	93.75	3,323	7.06
	WN	WN	1	3	2	93.91	2,670	7.54

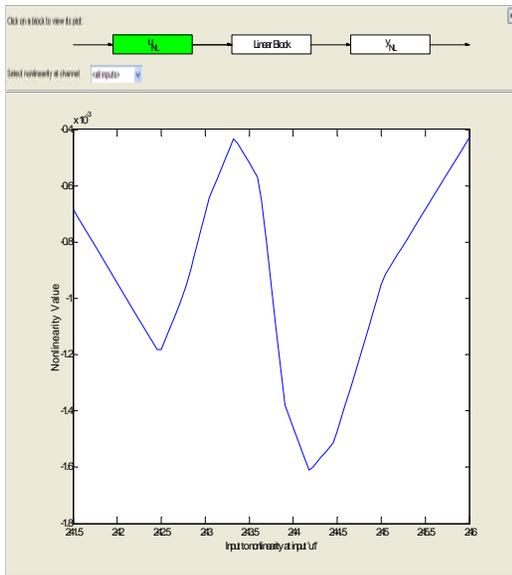
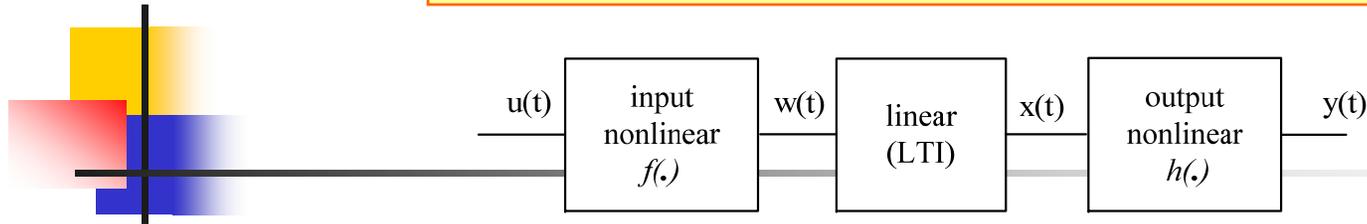
Compare Linear and Nonlinear Model

- Accuracy of Hammerstein-Wiener and Hammerstein Model more than Linear model
- Model order of Nonlinear Hammerstein-Wiener and Hammerstein Model lower than linear Model
- Accuracy of Linear system identification lower than Nonlinear model
- Model order of linear higher than nonlinear system identification

Result of Hammerstein-Wiener model

Data	Input/Output Nonlinear	Nb	nf	nk	Model order	% fit	FPE	AIC
Voltage	Deadzone	1	5	1	5	87.23	3,079.8	10.33
	Saturation	4	5	2	8	93.54	729.03	6.59
	Pwlinear	1	2	2	2	98.05	26.27	3.26
	Sigmoid	3	2	2	4	93.75	3,323	7.06
	Wavenet	1	3	2	3	98.01	2,670	7.54
Current	Deadzone	3	8	2	10	91.76	0.07	2.57
	Saturation	3	4	2	6	95.02	0.23	2.99
	Pwlinear	4	6	7	9	94.51	0.05	1.53
	Wavenet	9	17	2	25	93.22	19.08	15.19
	Sigmoidnet	5	8	3	12	91.68	25.61	18.14
Power	Deadzone	3	7	5	9	91.05	8,688.3	9.06
	Saturation	6	4	1	9	92.28	1,262.7	9.44
	Pwlinear	8	6	2	13	92.32	3,263	8.08
	Sigmoidnet	4	9	3	12	92.82	8,480	6,010
	Wavenet	5	7	2	11	93.62	2008	1429

System Analysis



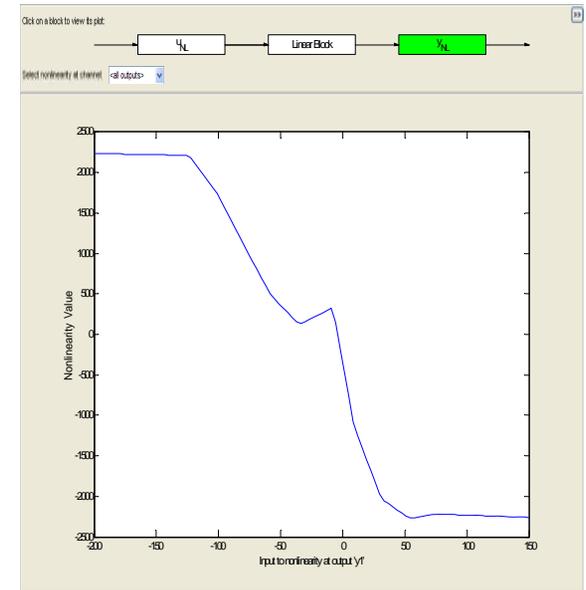
Input nonlinear

$$y(t) = \left[\frac{B(q)}{F(q)} \right] u(t) + e(t)$$

$$B(q) = q^2$$

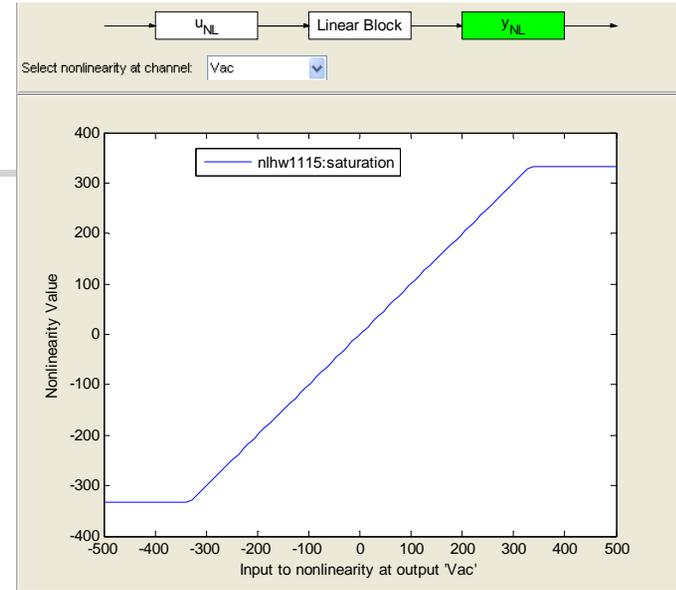
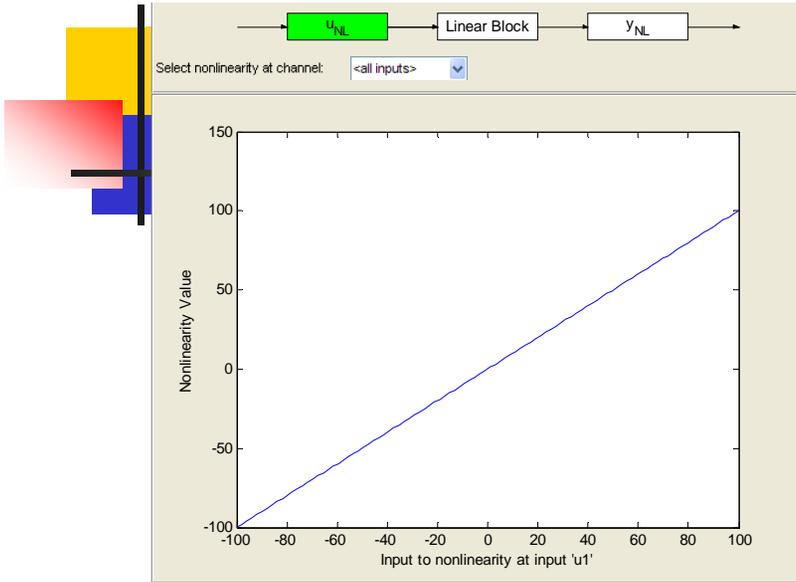
$$F(q) = 1 - 1.99q^{-1} + q^{-2}$$

Discrete polynomial model

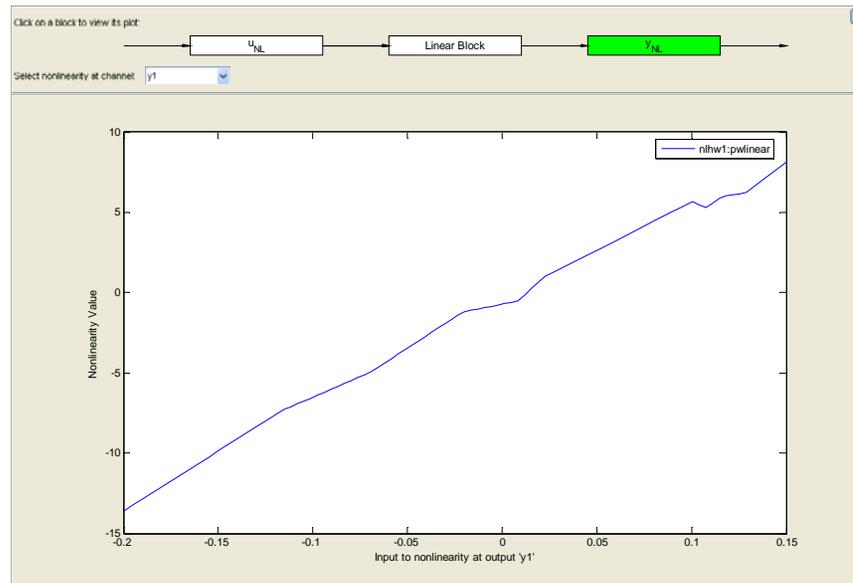


Output nonlinear

Nonlinear Estimator



Deadzone

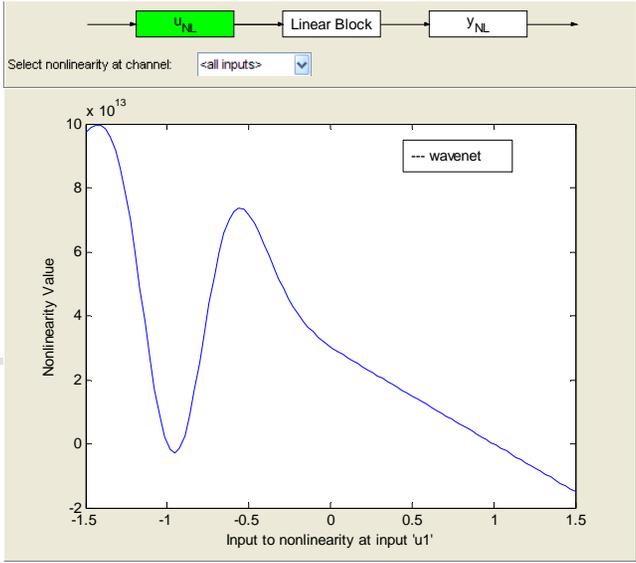


Saturation

piewiseliner

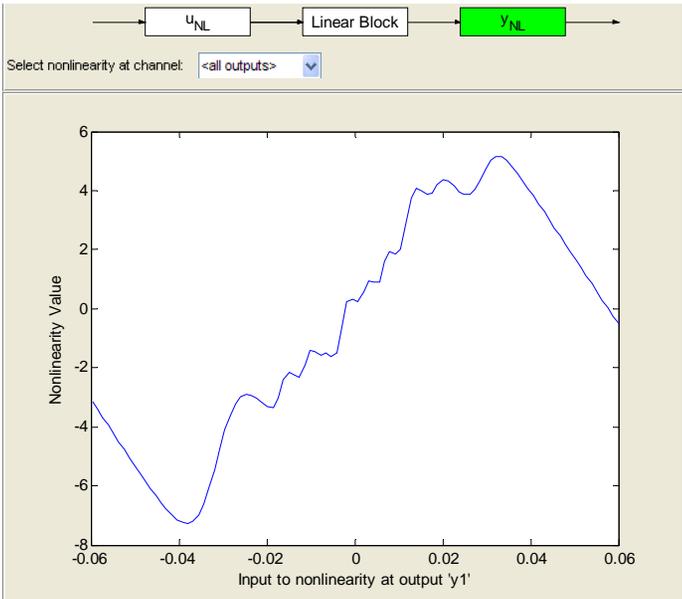
Properties	Input Nonlinear	Output Nonlinear
Regressor Mean	0.0052	-9.61×10^{-17}
NonLinear Subspace	1	1
Linear Subspace	1	1
Linear Coef	-0.1387	-6.1046
Dilation	[1x10 double*]	[1x10 double]
Translation	[1x10 double]	[1x10 double]
Output Coef	[10x1 double]	[10x1 double]
Output Offset	-0.0527	1.1208

wavenet

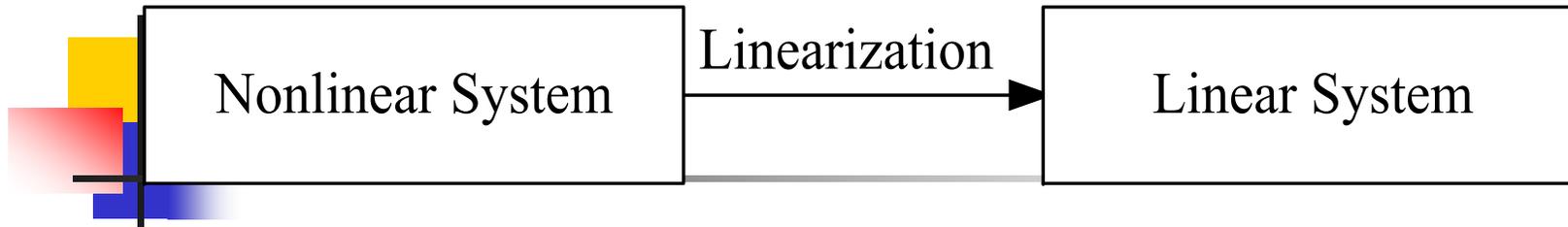


Properties	Input Nonlinear	Output Nonlinear
Number of Unit	6	11
Regressor Mean	- 8.5126	-98.55
Nonlinear Subspace	0.0056	4.58e-4
Linear Subspace	0.0056	4.58e-4
Output Offset	-7.0973	-0.4855
Linear Coef	176.51	3.1140
Scaling Coef	[0x1 double*]	[3x1 double]
Wavelet Coef	[6x1 double]	[8x1 double]
Scaling Dilation	[0x1 double]	[3x1 double]
Wavelet Dilation	[6x1 double]	[8x1 double]
Scaling Translation	[0x1 double]	[3x1 double]
Wavelet Translation	[6x1 double]	[8x1 double]

Sigmoidnet



Linear System analysis



State space equation

$$x(t + Ts) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

$$A = \begin{bmatrix} 1.99 & 1 & -1.486e-5 \\ -0.99 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix} \quad C = [1 \quad 0 \quad 0]$$

$$D = [0 \quad 12.99]$$

Transfer function

$$G(z) = \frac{-1.486e-5}{z^2 - 1.999z + 0.996}$$

Gain = $-1.486e-5$

zero = 0

pole = $0.997 - 0.0159i$
 $= 0.997 + 0.0159i$

Linear System analysis

Nonlinear System

Linearization

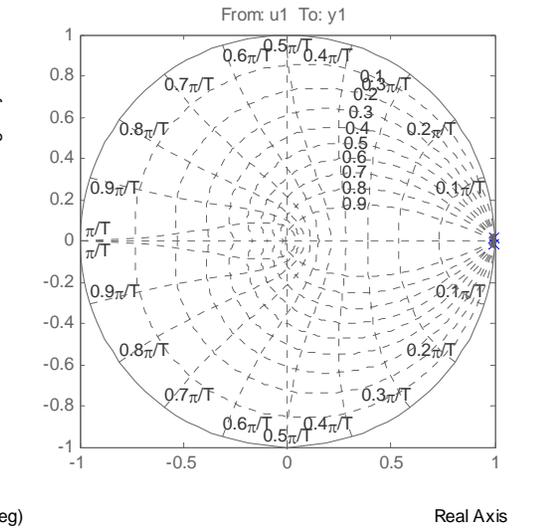
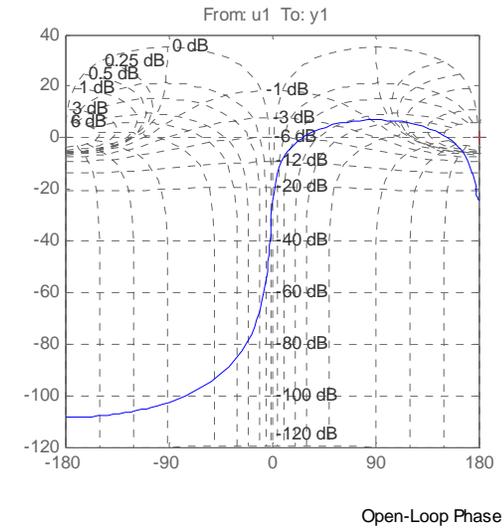
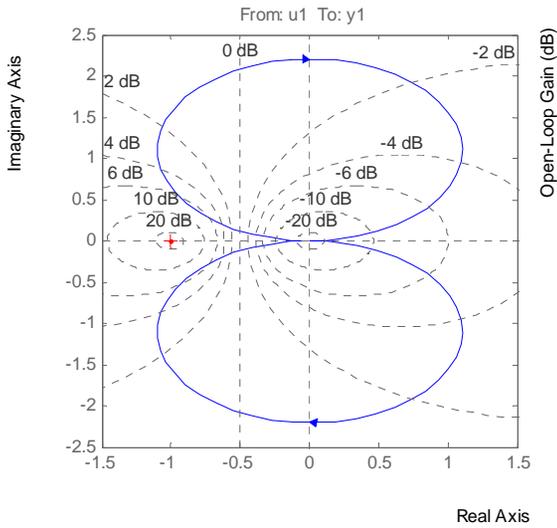
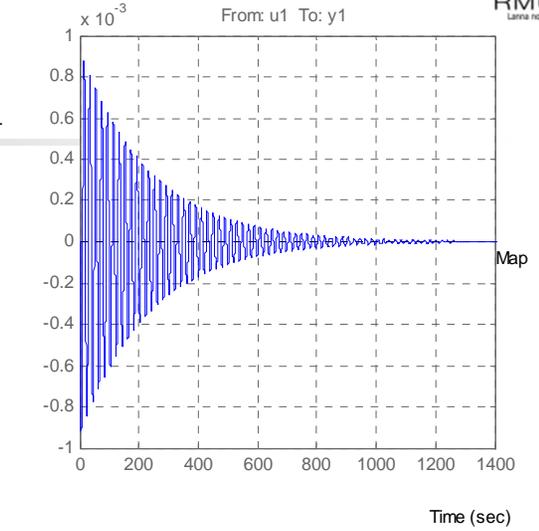
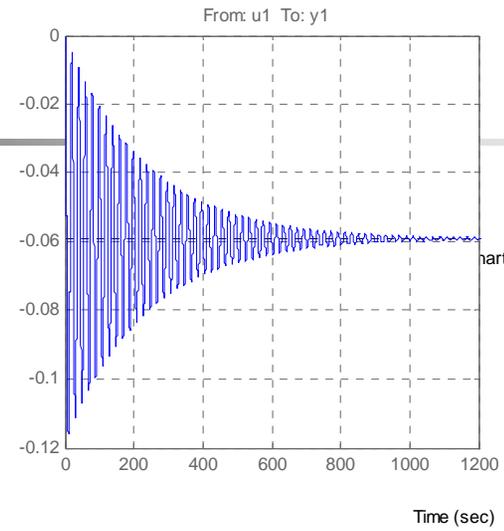
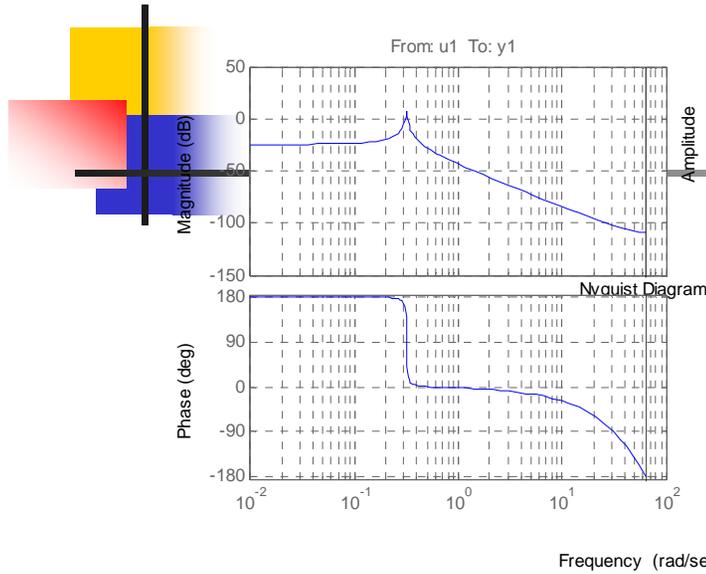
Linear System

$$B(q) = 1.025q^{-5} - 1.635q^{-6} + 0.1838q^{-7} + 0.4257q^{-8}$$

$$F(q) = 1 - 2.396q^{-1} + 1.794q^{-2} - 0.3979q^{-3}$$

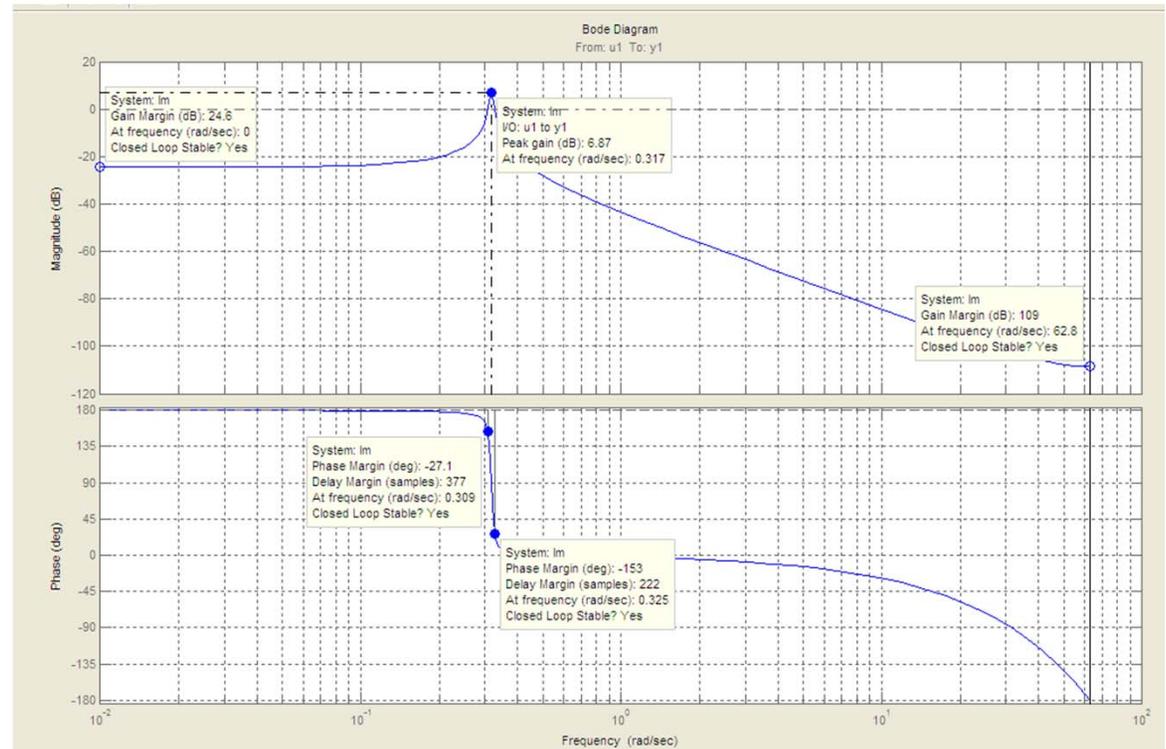
$$G(z) = \frac{1.025z^3 - 1.635z^2 + 0.183z + 0.425}{z^8 - 2.395z^7 + 1.794z^6 - 0.397z^5}$$

Graphical Tool for analysis

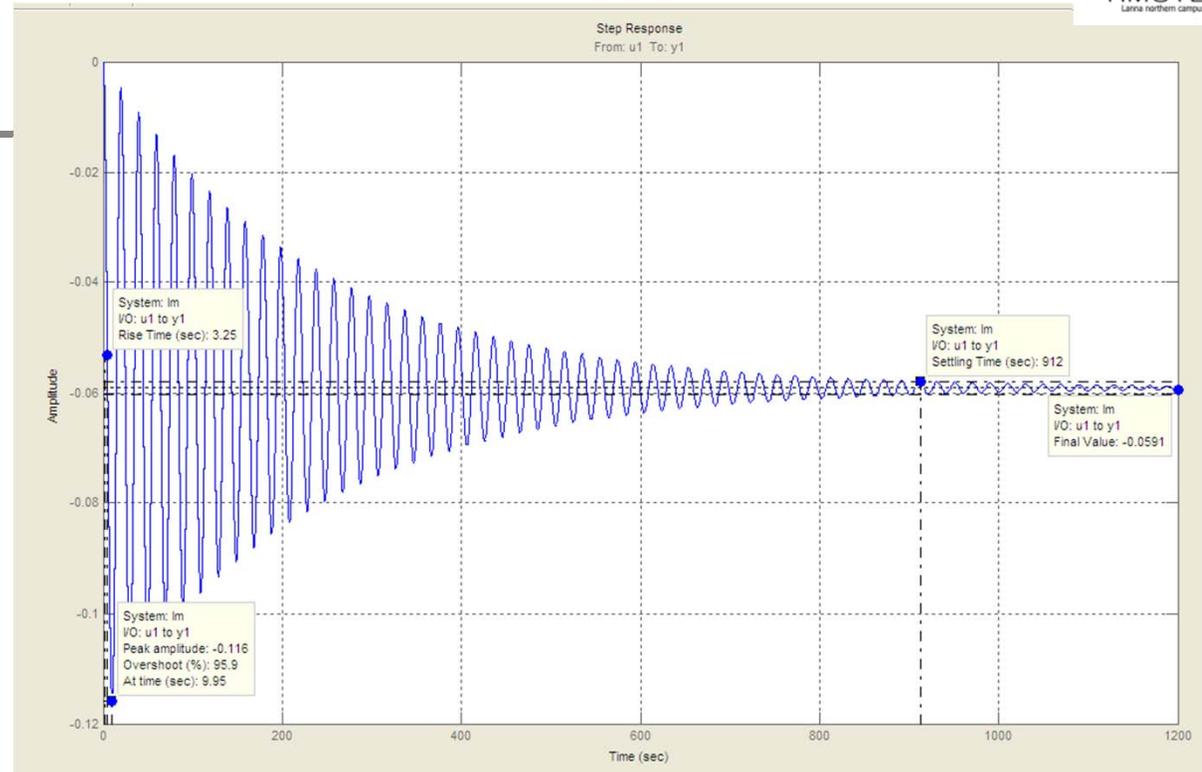


Bode plot

- Peak gain Value 6.87 dB at frequency 0.317 rad/sec
- Gain Margin 2 value 24.6 dB at frequency 0 rad/sec and 109 dB at frequency 62.8 rad/sec
- Phase Margin -27.1 at frequency 0.309 rad/sec

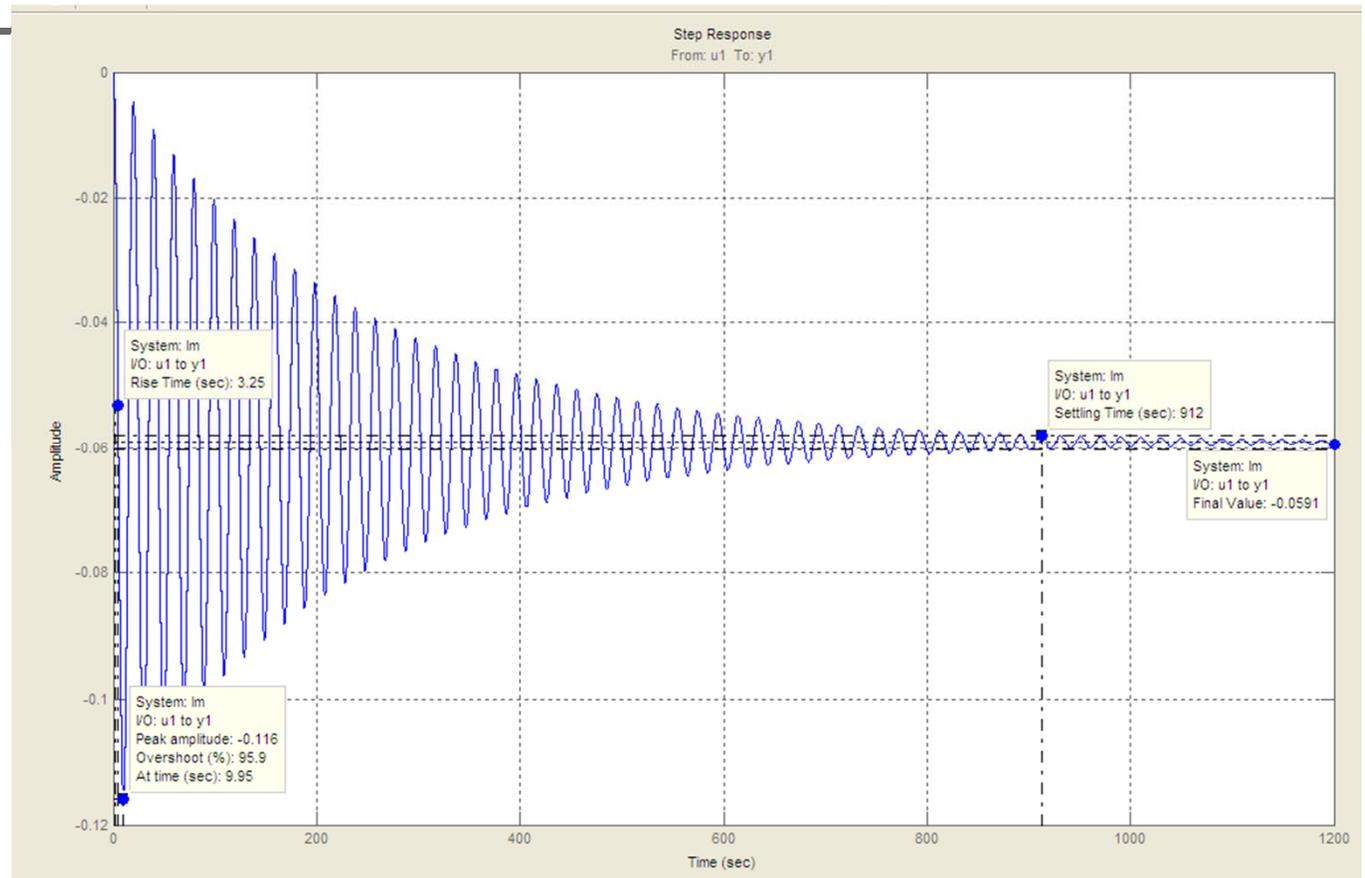


Step response



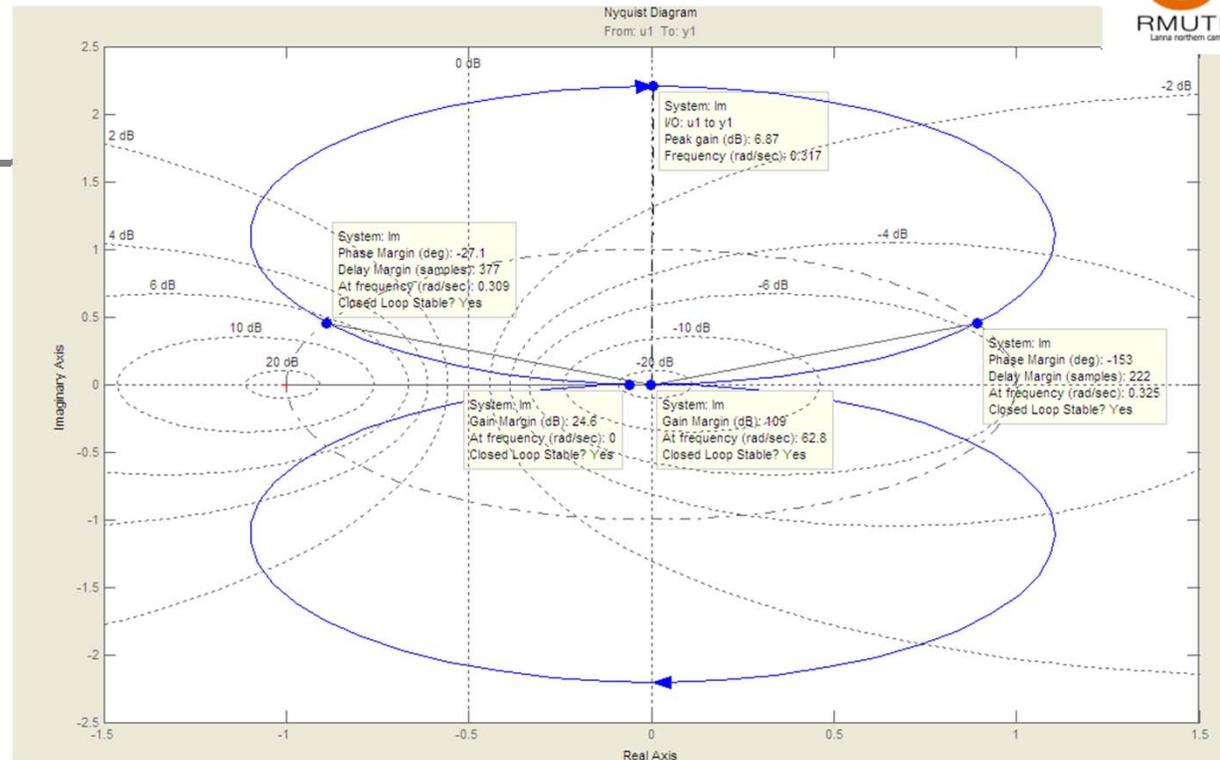
- When we feed unit step input
- rise time, t_r 3.25 Second
- peak time, t_p 9.95 Second Maximum - 0.116
- maximum overshoot 95.9%
- settling time, t_s 912 Second and final magnitude 0.059

Impulse response



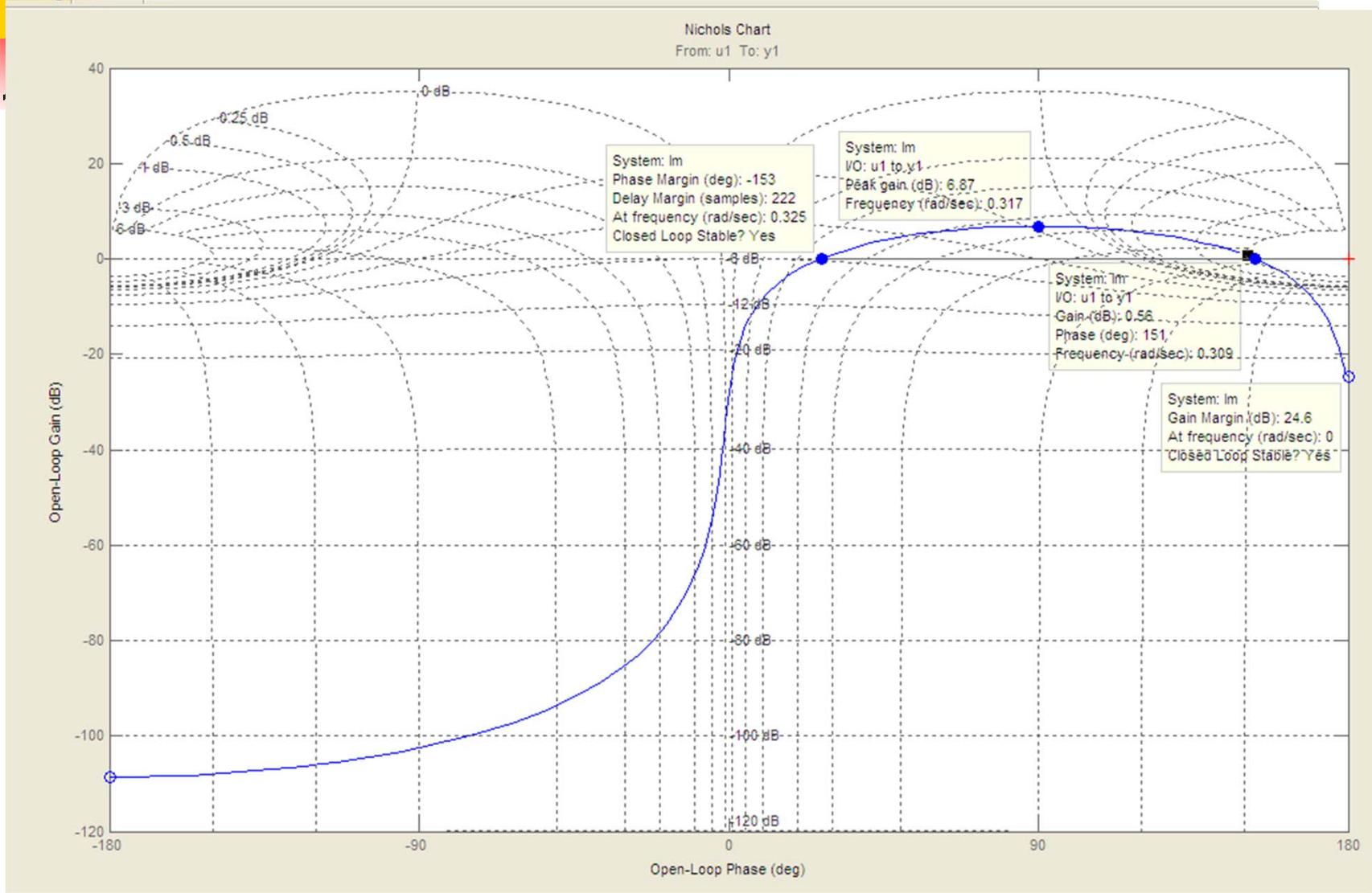
- Amplitude -0.000915 at time 4.95 and steady state time 917 second

Nyquist Analysis



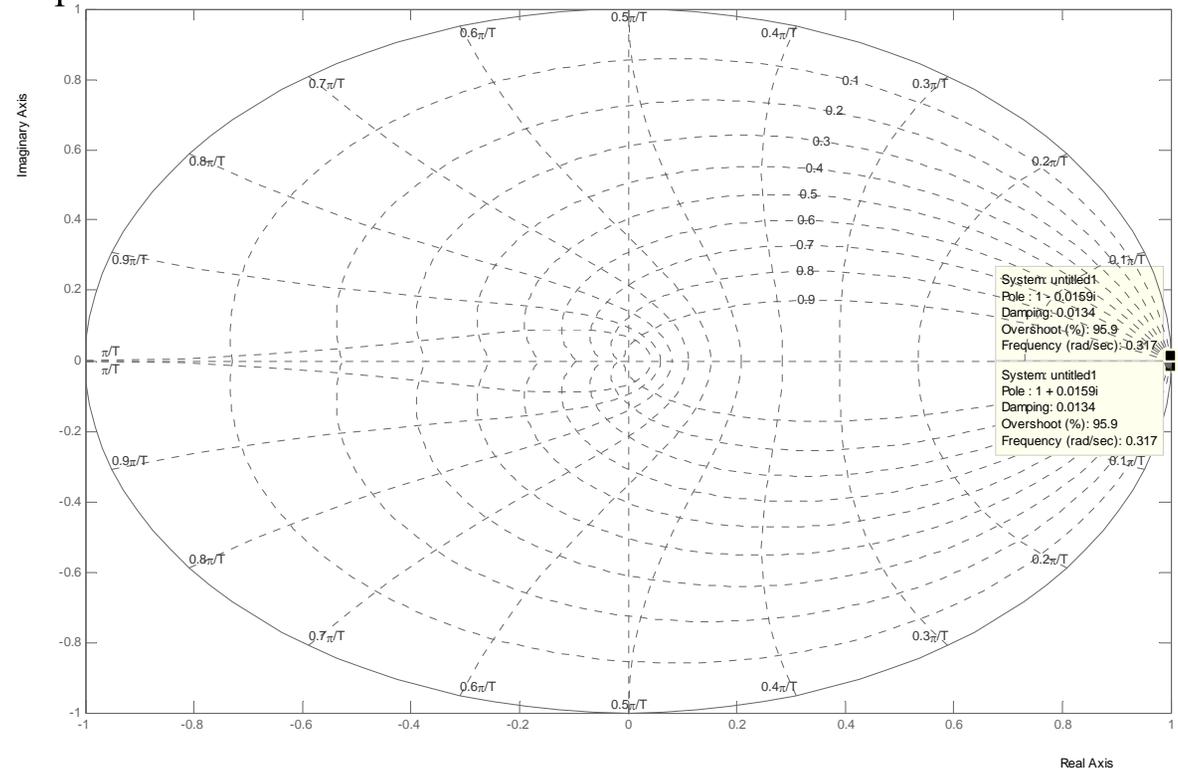
- Peak gain = 6.87 dB at frequency 0.317 rad/s
- Gain margin 2 values are 24.6 dB at frequency 0 rad/sec and 109 dB at frequency 62.8 rad/sec
- Phase margin 2 values are -27.1 degree at frequency 0.309 rad/sec and -153 degree at frequency 0.325 rad/sec

Nichols plot



Pole zero map

- Pole Position at $1-0.0159i$ and Zero Position at $1+0.0159i$
- damping 0.0134 , overshoot 95.9% at frequency 0.317 rad/sec
- Stability Analysis found that pole position locate in unit circle



Linear system Stability analysis

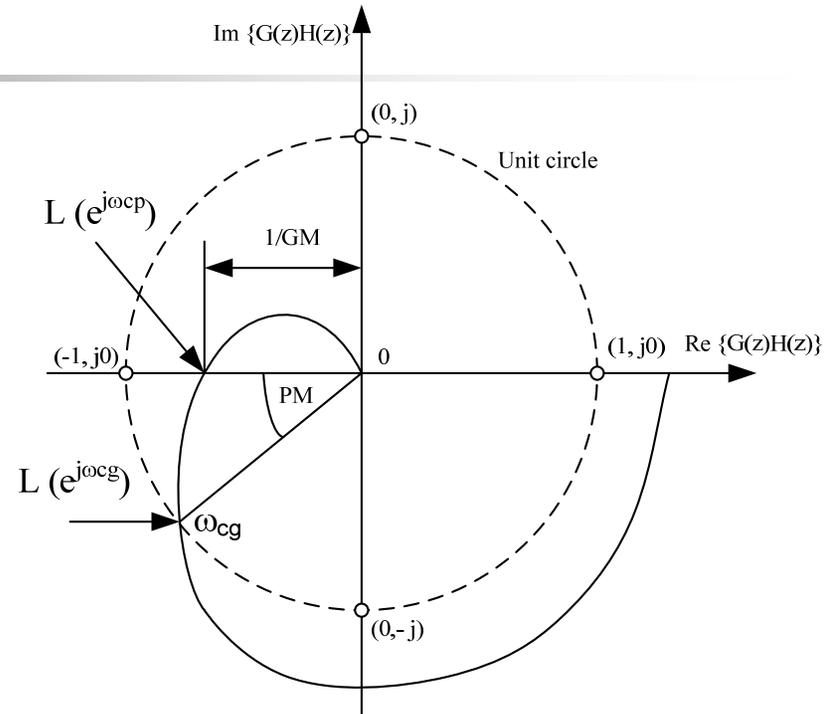
- Nonlinear \rightarrow Linear
- Linearization around operating point
- Steady State condition
- Stability analysis

Linear system Stability analysis

- Right hand plane (RHP)
- Root locus, Routh – Hurwitz criterion
- Z plane and Unit circle
- Eigenvalue of Jacobian matrix
- Lyapunov
- **Bode-Nyquist stability criterion**

Bode-Nyquist stability criterion

- gain margin (GM)
- phase margin (PM)
- gain crossover frequencies
- phase crossover frequencies



SISO Stability Criterion

$$1 \approx 0 \text{ dB} < GM < 4 \approx 12 \text{ dB and } 30 < PM < 60$$

$$Pm = 180 + \arg L(e^{j\omega})$$

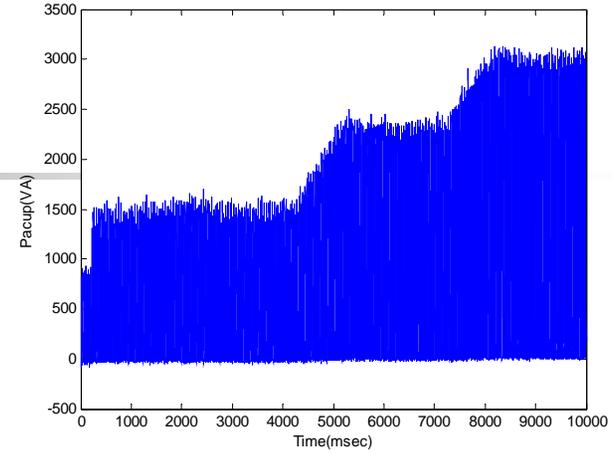
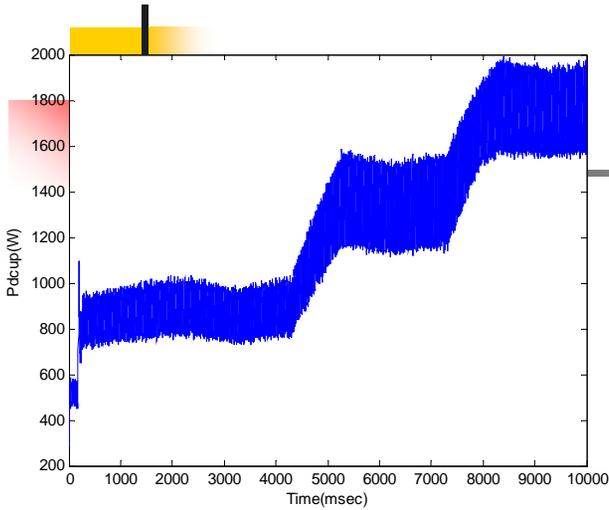
$$Gm = \frac{1}{|L(e^{j\omega_{cp}})|} = \frac{1}{|Re\{e^{j\omega}\}|}$$

- Modeling System in Steady state
- **Modeling System in Transient**
- Modeling System in Islanding
- Modeling System with cross validation
- Modeling with MIMO model

Experimental for Transient Condition

Electrical parameter	Step Up		Step Down	
	AC Voltage output (V)	220	220	220
AC Current output (A)	7	2	2	7
AC Power output (W)	1540	440	440	1540

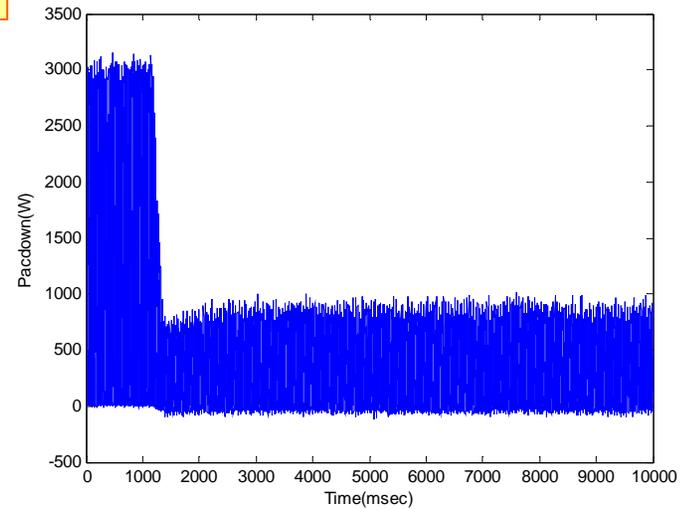
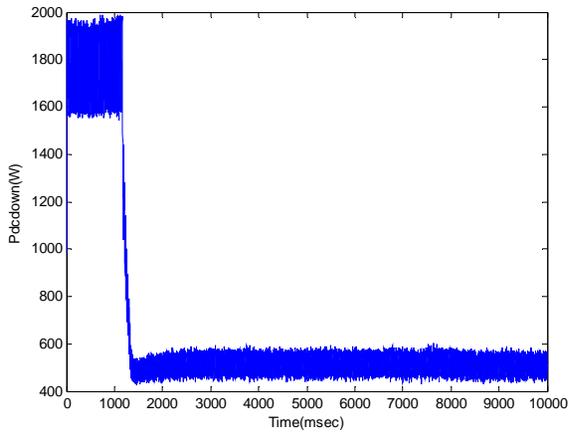
Step up condition



Power dc input

Power ac output

Step down condition



Power dc input

Power ac output

Model properties and comparison of waveform

Step Up Condition

Nonlinear	Linear Parameters			Model Properties			
	I/P & O/P	nb	nf	nk	model	% fit	FPE
Deadzone	3	4	2	6	91.75	3,230	7.40
Saturation	4	3	2	6	83.46	3256	11.34
Pwlinear	4	4	5	7	87.20	4720	8.38
Sigmoidnet	3	5	5	7	83.85	4238	8.43
Wavenet	4	5	2	8	84.57	2980	9.52

Model properties and comparison of waveform

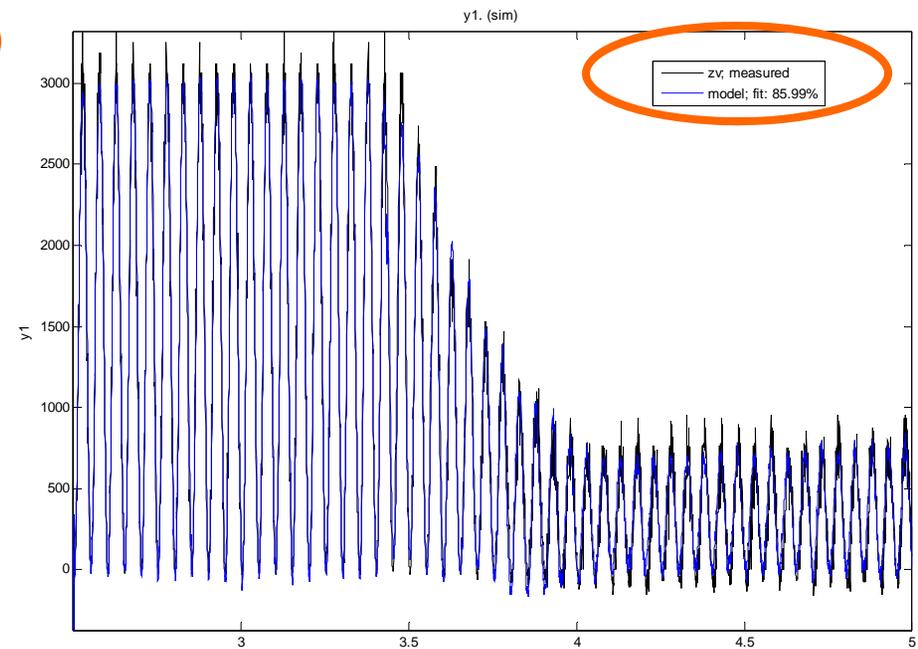
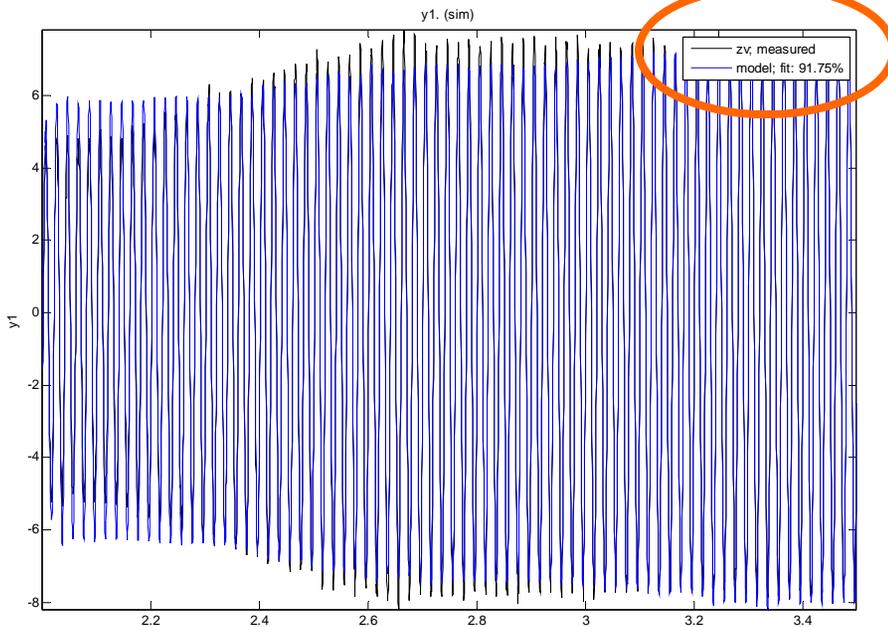
Step Down Condition

Nonlinear	Linear Parameters			Model Properties			
	I/P & O/P	nb	nf	nk	model	% fit	FPE
Deadzone	4	5	5	8	85.12	9,718	9.18
Saturation	3	5	5	7	81.29	3049	11.23
Pwlinear	3	4	3	6	85.99	3233	10.0
Sigmoidnet	4	4	1	7	81.17	4426	8.28
Wavenet	4	5	4	8	82.45	3325	9.25

Simulation Result for Transient

Step up condition

Step down condition



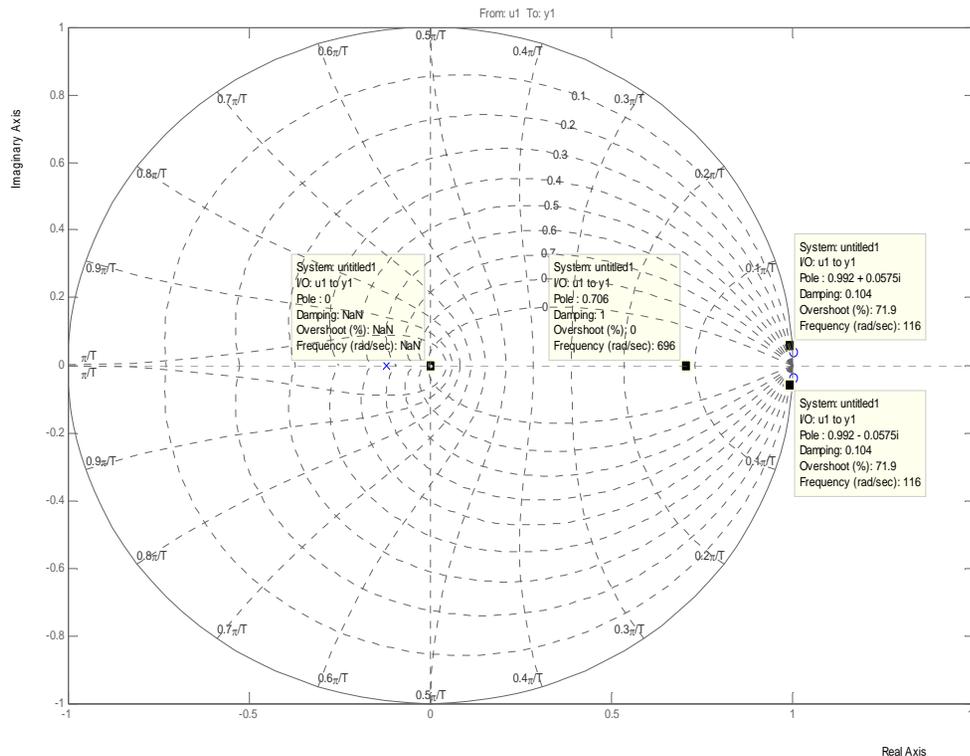
Stability Analysis

Stability : consider from pole position, magnitude of pole and unit circle•

Pole 4 position follow as

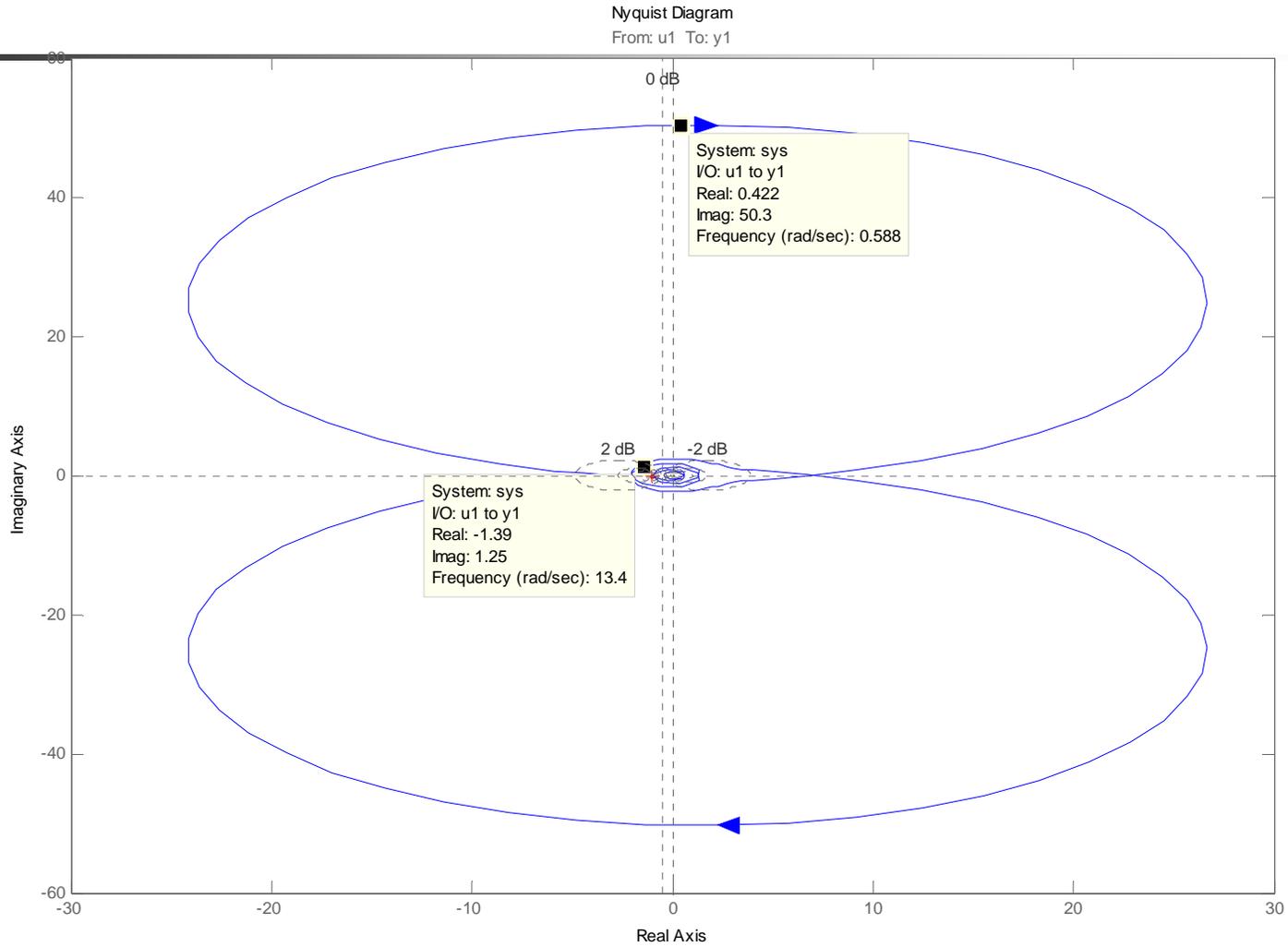
$$0.9923 + 0.0575i, 0.9923 - 0.0575i, 0.7060 \text{ and } -0.1213$$

Magnitude are 0.9940, 0.9940, 0.7060 and 0.1213•



Magnitude of pole < 1
All Pole locate in unit circle
: System is stable

Linear Stability analysis

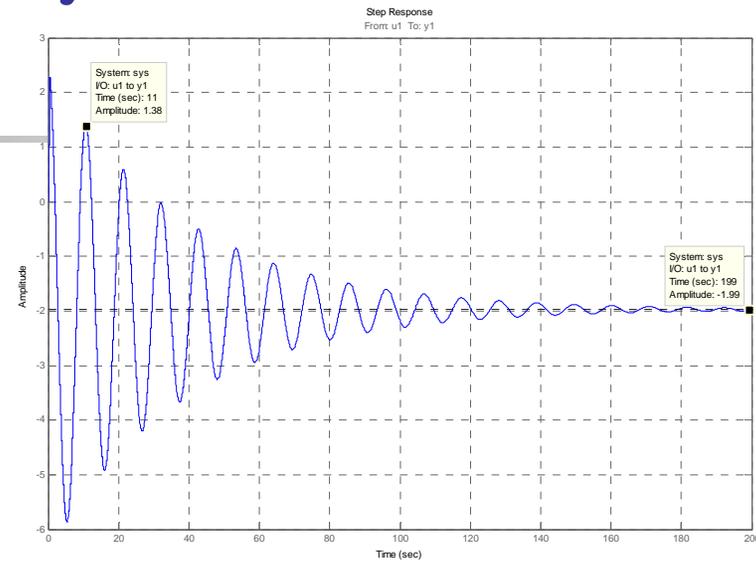


Linear Stability analysis

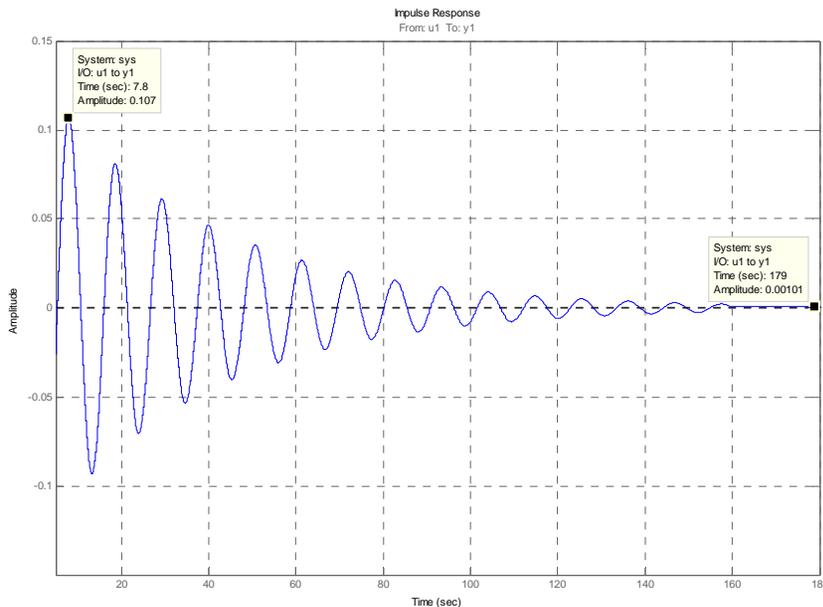
Criteria	Condition	Result	Stability
Gain Margin (GM)	$0 < GM < 4$	0.679 dB	Stable
Phase Margin (PM)	$30 < PM < 60$	31.8	Stable

Absolute stability analysis

Criteria	Result
Rise Time	5.2 sec
Settling Time	206 sec
Overshoot	95.9%



Step Response

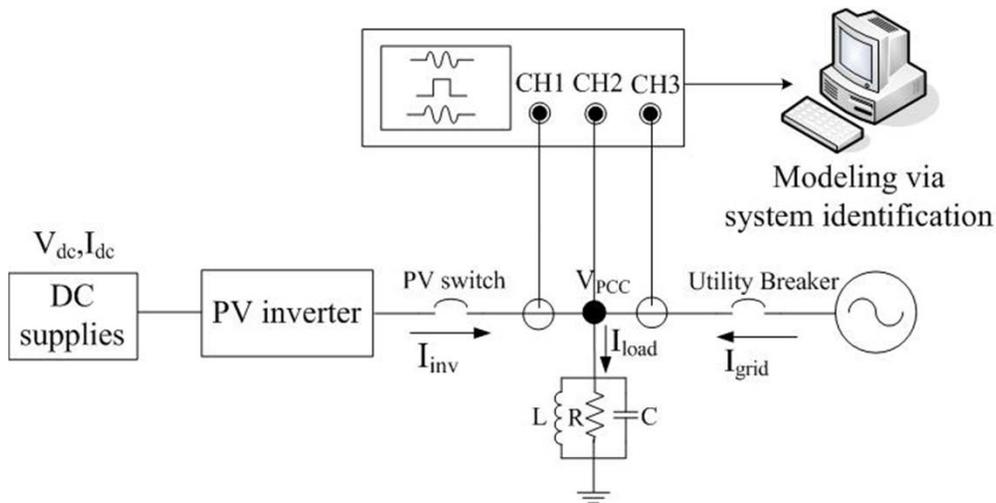
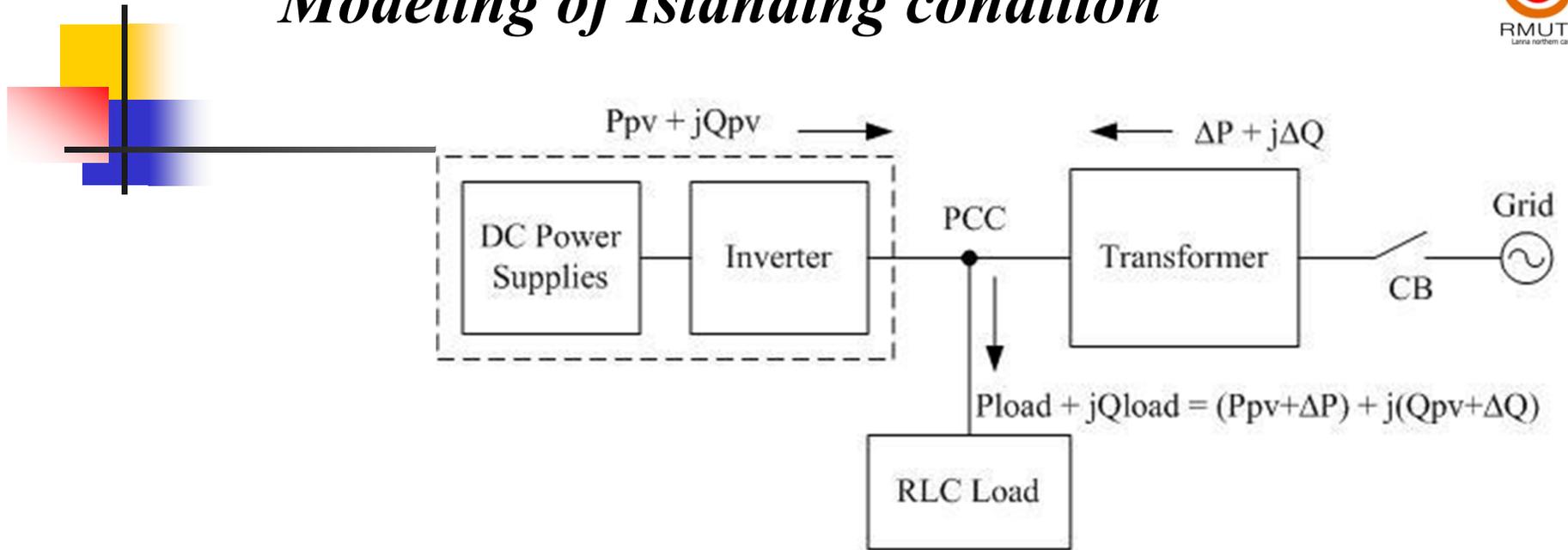


Impulse Response

Topic for Experimental and Modeling

- Modeling System in Steady state
- Modeling System in Transient
- Modeling System in Islanding
- Modeling with MIMO model

Modeling of Islanding condition

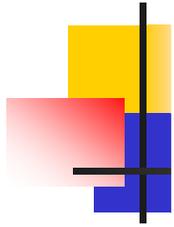
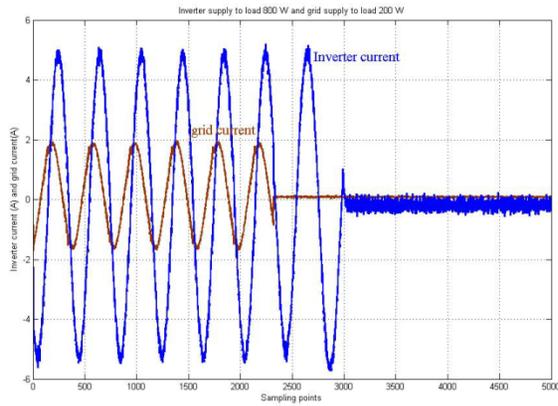


Design Simulation in Six Condition of Islanding

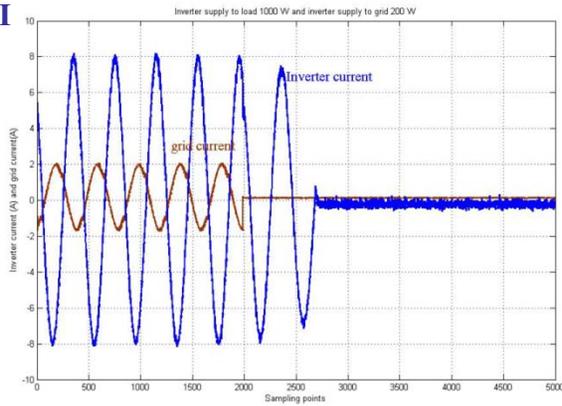
No	Model input	$P_{inverter}$	P_{load}	P_{grid}	Load
		(W)	(W)	(W)	
I	Grid current	1,000	800	-200*	R
II	Grid current	1,200	1,000	200	R
III	Grid current	1,000	1,000	-	RLC
IV	PCC voltage	1,000	800	-200	R
V	PCC voltage	1,200	1,000	200	R
VI	PCC voltage	1,000	1,000	-	RLC

* sign (-) mean grid current energize power into the load

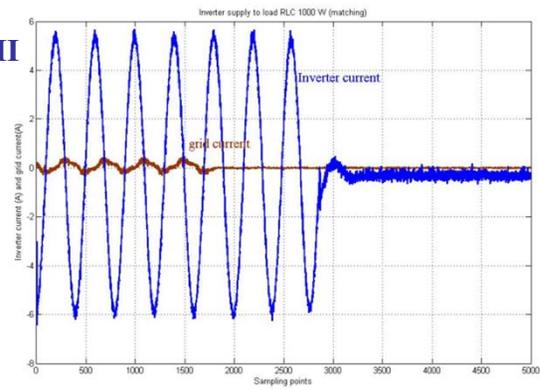
Scenario I



Scenario II

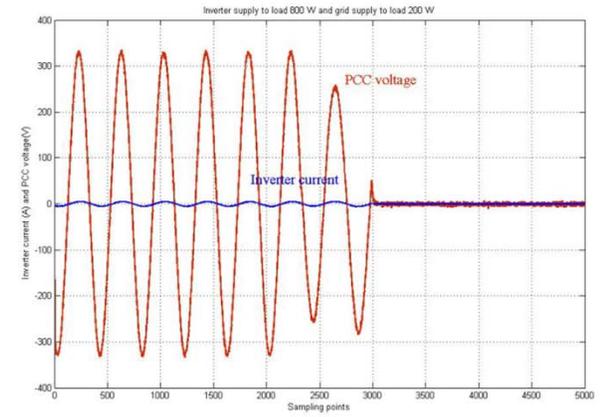


Scenario III

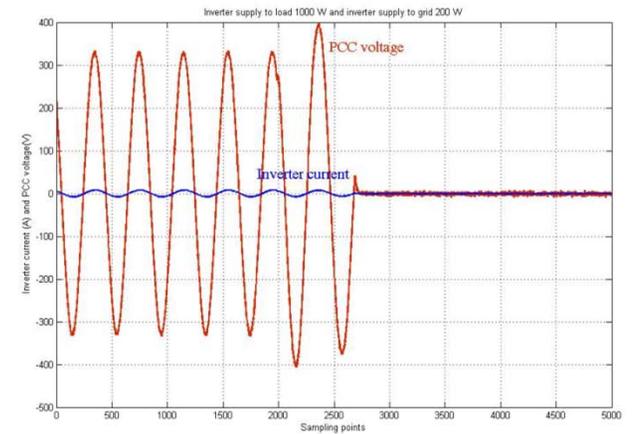


Grid current input

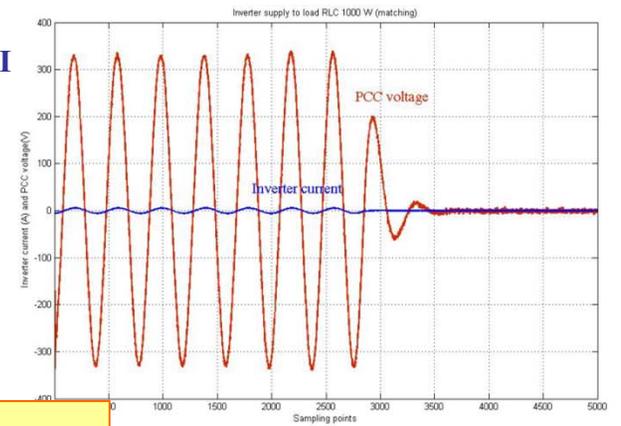
Scenario IV



Scenario V



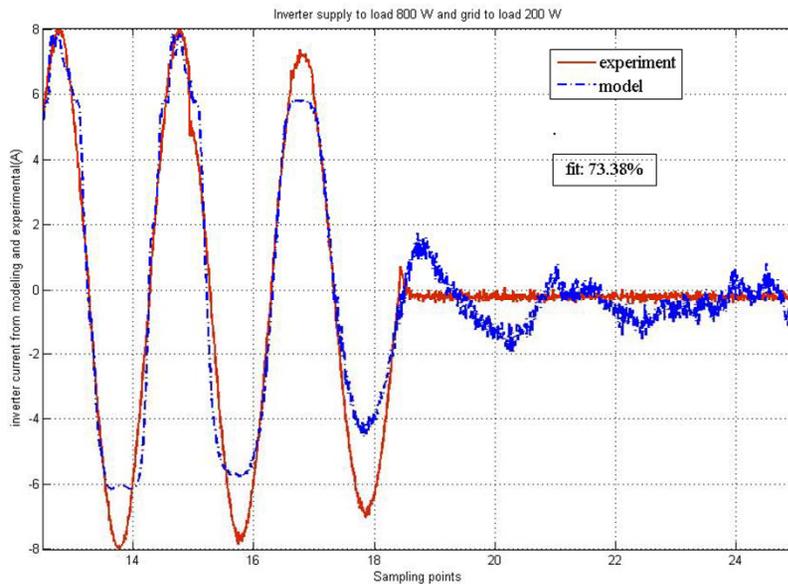
Scenario VI



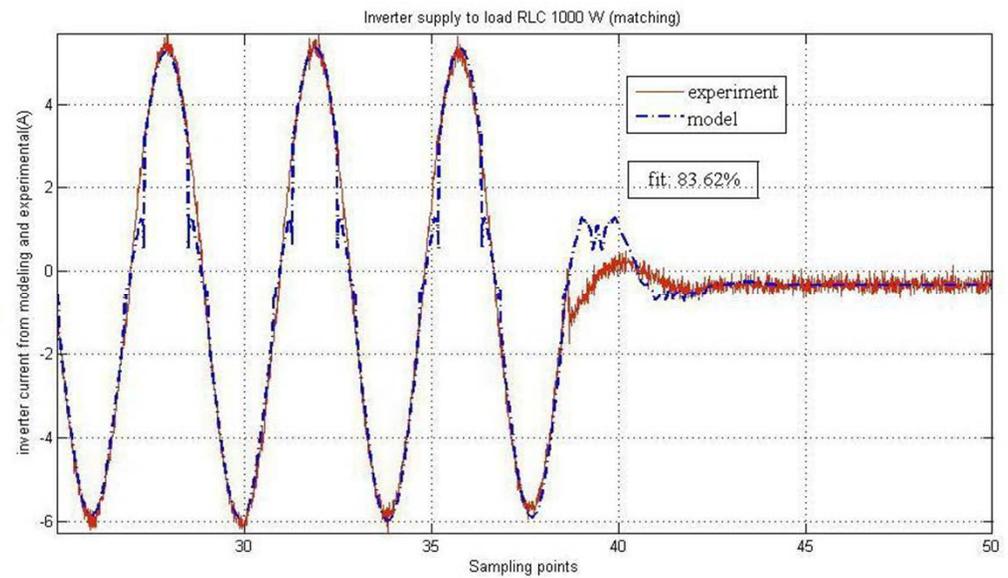
PCC voltage

The Input and output of model

Simulation Result in condition 1 and 6



scenario I

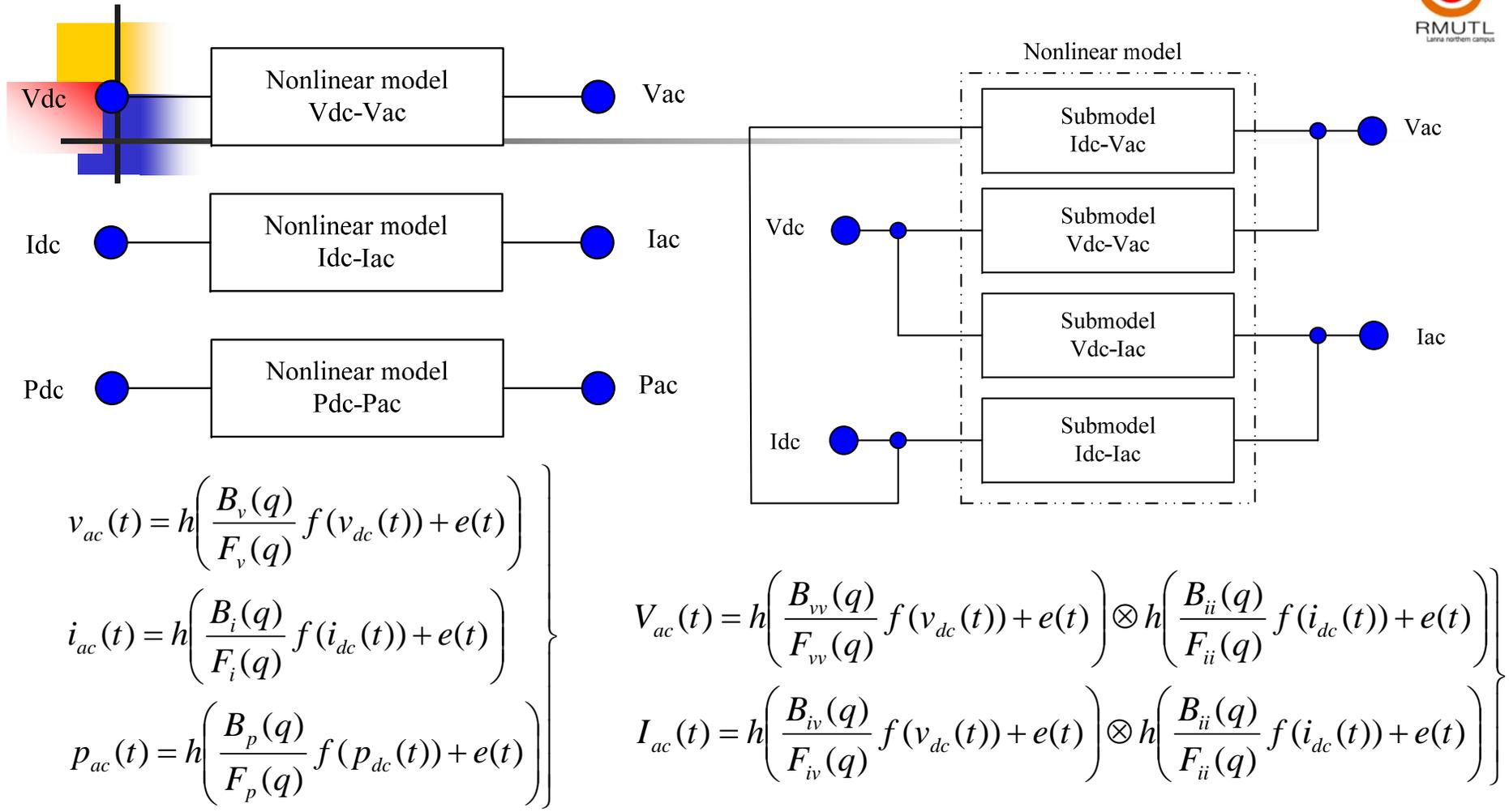


scenario VI

Topic for Experimental and Modeling

- Modeling System in Steady state
- Modeling System in Transient
- Modeling System in Islanding
- Modeling with MIMO model

MIMO (Multi Input Multi Output) Model



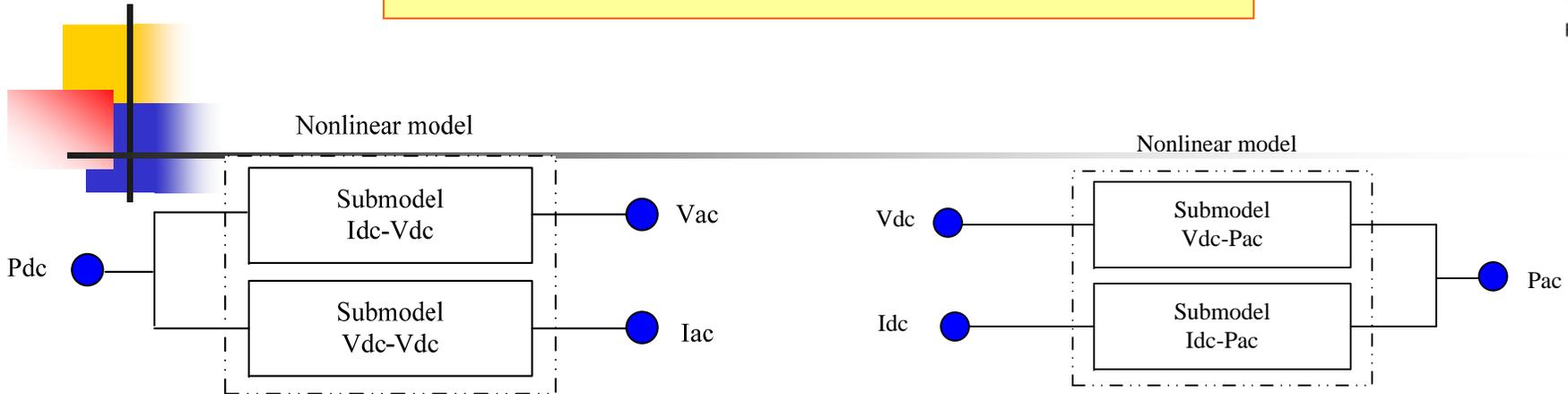
Single input single output (SISO) model

Multiple input multiple output (MIMO) model

= 3x n = 3x 1 = 3

= 3x n = 3x4 = 12

Structure of Model



$$\left. \begin{aligned} V_{ac}(t) &= h \left(\frac{B_v(q)}{F_v(q)} f(P_{dc}(t)) + e(t) \right) \\ I_{ac}(t) &= h \left(\frac{B_i(q)}{F_i(q)} f(P_{dc}(t)) + e(t) \right) \end{aligned} \right\}$$

Single input multiple output (SIMO) model

$$= 3 \times n = 3 \times 2 = 6$$

$$p_{ac}(t) = h \left(\frac{B_v(q)}{F_v(q)} f(v_{dc}(t)) + e(t) \right) \otimes h \left(\frac{B_i(q)}{F_i(q)} f(i_{dc}(t)) + e(t) \right)$$

Multiple input single output (MISO) model

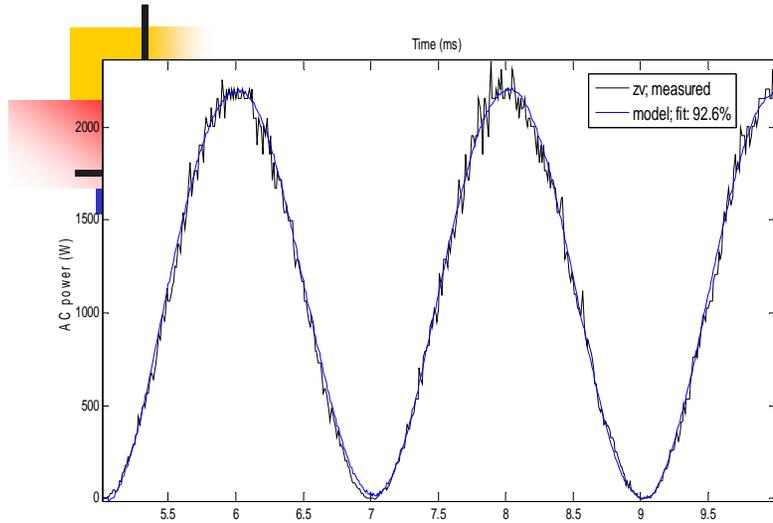
$$= 3 \times n = 3 \times 2 = 6$$

Number of linear parameter (nb nf nk)

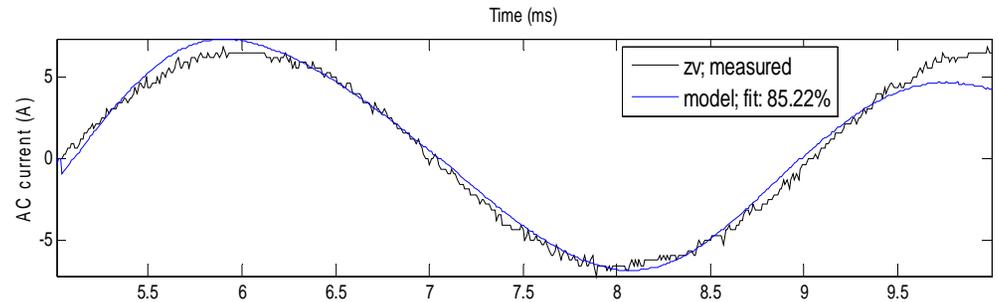
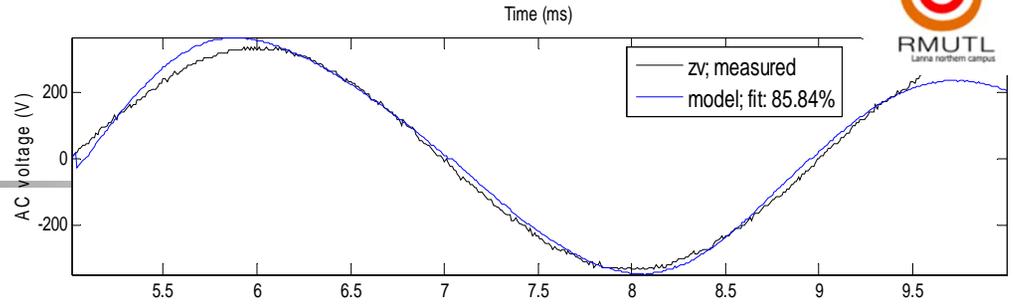
$$= 3 \times n ; n = \text{submodel}$$

Result of MIMO Model

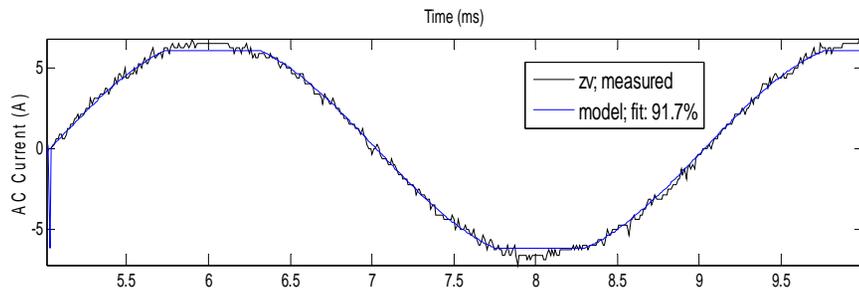
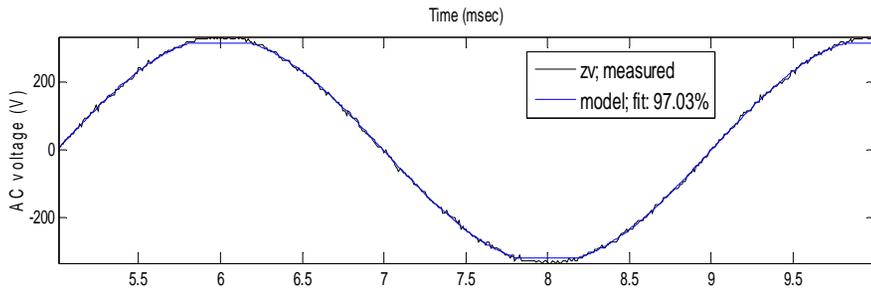
Type	I/P	O/P	Linear [nb];[nf] [nk];	% fit	FPE	AIC
MISO	DZ	DZ	[2 4]; [6 3]; [4 4]	92.60	63,034	11.35
	ST	ST	[2 2]; [2 3]; [3 3]	89.06	31,559	10.35
SIMO	DZ	DZ	[4 4]; [3 2]; [3 2]	85.84 85.22	155.45	5.04
	ST	ST	[3 4]; [5 2]; [2 2]	95.12 91.23	27.71	3.32
MIMO	DZ	DZ	[4 4 3 5]; [5 5 3 6]; [3 4 4 2]	87.34 84.15	254.45	7.89
	ST	ST	[3 5 4 5]; [4 5 4 3]; [4 4 4 2]	97.03 91.70	175.43	6.35



MISO power output

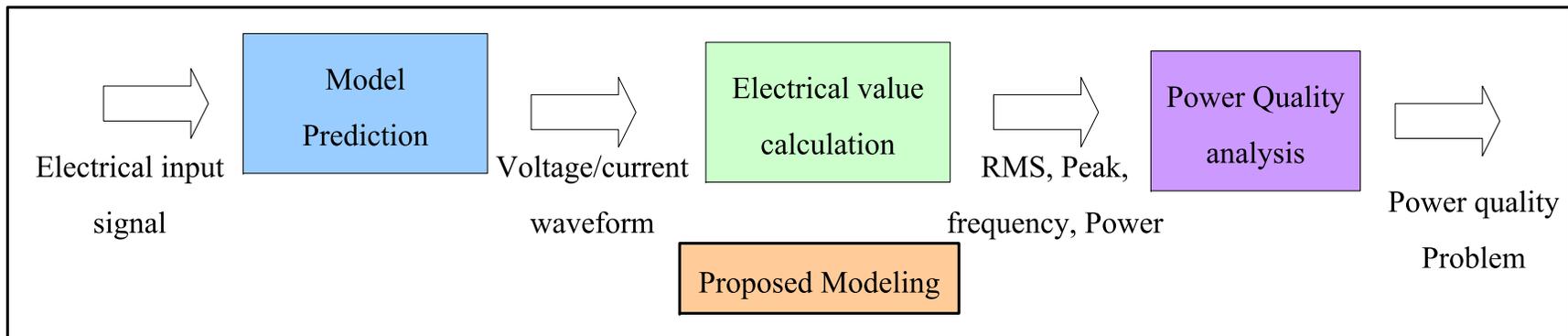
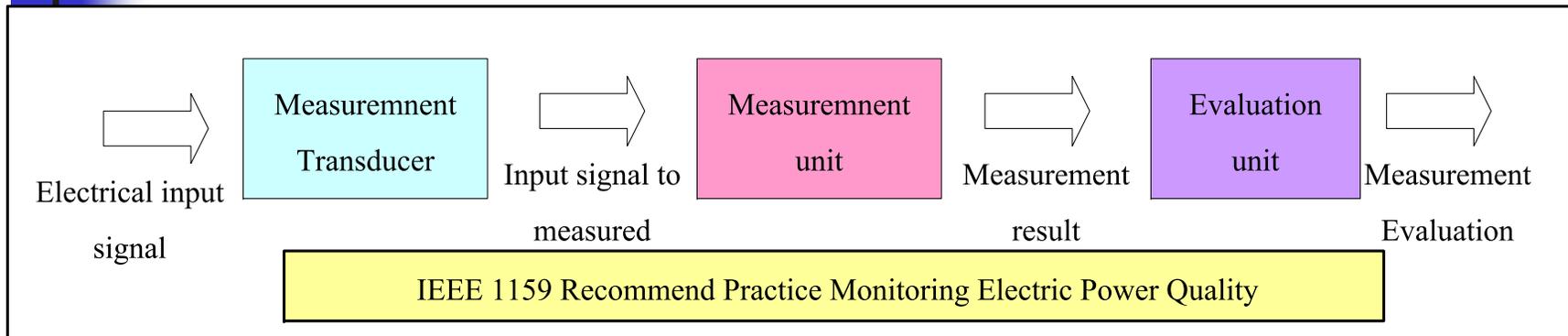


SIMO voltage and current output

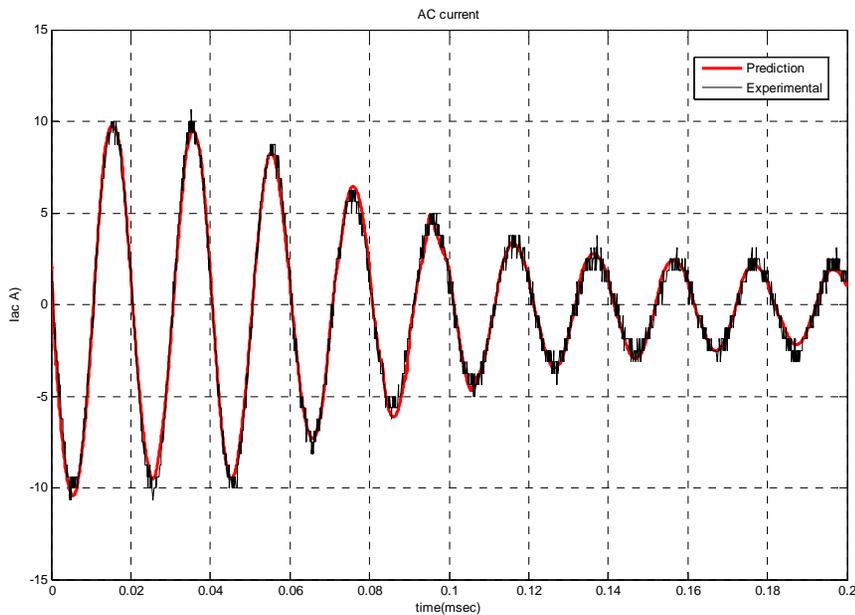


MIMO voltage and current output

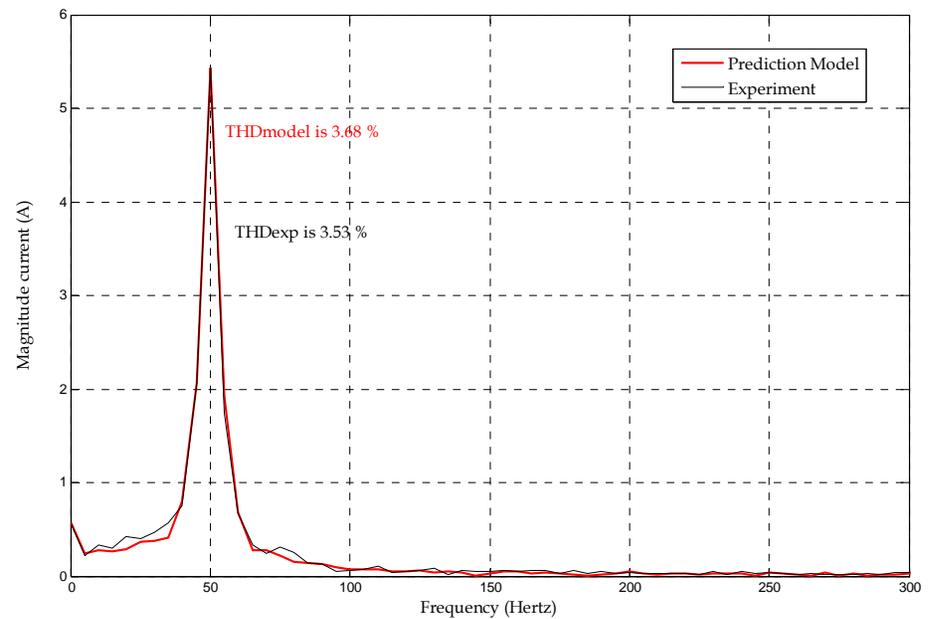
Method for Power Quality Analysis from measurement and Modeling



Simulation and Experimental for Power Quality Analysis



Model output



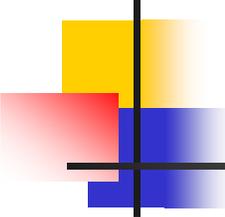
Total Harmonic Distortion output

Power Quality Analysis in Steady State and Transient Condition

Parameter	Steady state FVHC condition			Transient step down condition		
	Experimental	Modeling	% Error	Experimental	Modeling	% Error
Vrms (V)	218.31	218.04	0.12	217.64	218.20	-0.26
Irms (A)	23.10	23.21	-0.48	4.47	4.45	0.45
Frequency (Hz)	50	50	0.00	50.00	50.00	0.00
Power Factor	0.99	0.99	0.00	0.99	0.99	0.00
THDv (%)	1.15	1.2	-4.35	1.18	1.24	-5.08
THDi (%)	3.25	3.12	4.00	3.53	3.68	-4.25
S (VA)	5044.38	5060.7	-0.32	972.85	970.99	0.19
P (W)	4993.94	5010.1	-0.32	963.12	961.28	0.19
Q (Var)	711.59	713.85	-0.32	137.24	136.97	0.19
V p.u.	0.99	0.99	0.00	0.98	0.99	-1.02

Model Application and Future Research

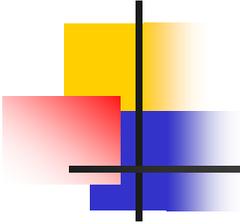
- Gray box system identification
 - Recursive system identification – Kalman filtering
 - Model predictive control
 - Model order reduction – Robust control
 - Power Quality Analysis from Modeling
 - Voltage Stability Analysis from Modeling
 - Load flow and penetration analysis from Modeling
- Increase accuracy
and Real time modeling
- Control base on Modeling
- Power Quality Issue
from Modeling



Conclusion

- A model of a PV inverter has been experimentally obtained from the Nonlinear Hammerstein-Wiener method.
- The model consists of three parts, static input and output parts, and dynamic middle part.
- The obtained model is validated and compared with the experimental results.
- The dynamic stability behavior of the system has been analyzed through the linearized version of the system using a frequency response analysis.
- Power Quality Analysis of output system can be done by using modeling and standard

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Thank you for you attention

